

# Air Quality Permitting Technical Memorandum

January 22, 2003

### Tier II Operating Permit and Permit to Construct No. 077-00023 Chevron Pipeline Company, Pocatello, Idaho

Project No. T2-010301

Prepared by:

Michael Stambulis, P.E., Staff Engineer State Office of Technical Services

**FINAL PERMIT** 

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#### ACRONYMS, UNITS, AND CHEMICAL NOMENCLATURE

AFS AIRS Facility Subsystem

AIRS Aerometric Information Retrieval System

AP-42 Compilation of Air Pollutant Emissions Factors, Volume J: Stationary Point

and Area Sources

AQCR Air Quality Control Region
CFR Code of Federal Regulations

CO carbon monoxide

DEQ Department of Environmental Quality

EPA United States Environmental Protection Agency

gal/yr gallons per year

HAP Hazardous Air Pollutant

IDAPA Idaho Administrative Procedures Act

L liter

m<sup>3</sup> cubic meter

MACT Maximum Available Control Technology

NESHAP Nation Emission Standards for Hazardous Air Pollutants

NO<sub>x</sub> nitrogen oxides

NSPS New Source Performance Standards

PM<sub>10</sub> particulate matter with an aerodynamic diameter of 10 micrometers or less

PSD Prevention of Significant Deterioration

PTC permit to construct

SIP State Implementation Plan

SO<sub>2</sub> sulfur dioxide T/yr tons per year µm micrometers

VDU Vapor Destruction Unit VOC volatile organic compound

#### **PURPOSE**

The purpose of this memorandum is to explain the legal and factual basis for this draft Tier II operating permit in accordance with IDAPA 58.01.01.400 and the inclusion of existing Permits to Construct in accordance with IDAPA 58.01.01.200, Rules for the Control of Air Pollution in Idaho.

DEQ staff has reviewed the information provided by the Chevron Pipeline Company regarding the operation of their facility located in Pocatello, Idaho. The permittee requested status as a synthetic minor source. The basis for qualifying as a synthetic minor source is the limitation of gasoline, diesel, and transmix throughput to the petroleum storage tanks and loading racks.

The permittee also requested to increase the permitted throughput of gasoline, diesel, and transmix products to the facility. The permit authorizes the facility to increase throughput of gasoline, diesel, and transmix by adding a drag reducing agent to the incoming pipeline to increase the product flow rate.

#### PROJECT DESCRIPTION

This project is for a renewed Tier II operating permit that creates state and federally enforceable limitations on the Pocatello facility's potential to emit VOCs. This permit qualifies the Chevron Pocatello facility as a "synthetic minor" for both VOC and HAP emissions. The permit limits VOC and HAP emissions from the storage tanks and loading racks to below the major facility threshold listed below:

- VOC emissions 100 T/yr, and
- HAPs emissions 10 T/yr for a single HAP and 25 T/yr for aggregated HAPs.

As a "synthetic minor" source, the Chevron Pocatello facility is not subject to Tier I permitting, pollutant registration, and registration fee payments for major facilities.

#### **FACILITY DESCRIPTION**

The Chevron Pipeline Company/Northwest Terminalling Company facility located in Pocatello, Idaho, began operation in 1963. Initially the entire facility belonged to Chevron, but in 1994, with the exception of the mainline and manifold, it was transferred to Northwest Terminalling Company. Chevron personnel continue to operate the entire facility.

The facility receives refined petroleum products via a single 8-inch pipeline. This pipeline is part of a pipeline system that originates in Salt Lake City, Utah. When product comes in to the facility, it is routed to one of the aboveground storage tanks. From the storage tanks, the product is transferred to tanker trucks. During the transfer, additives are added to the product. Additives are brought to the facility by truck and loaded into one of the onsite additive tanks.

The facility, as originally constructed, consisted of 17 aboveground petroleum storage tanks, two additive storage tanks, a truck loading facility, and associated piping. Since 1963, seven aboveground petroleum storage tanks and 11 aboveground additive tanks have been added to the original facility. In 1997, a vapor destruction unit was added to the truck loading operation.

#### SUMMARY OF EVENTS

- On February 28, 1994, DEQ issued Chevron a PTC for the addition of the diesel storage tanks No. 919 and No. 920.
- On June 6, 1994, DEQ issued another PTC to Chevron for the addition of the diesel storage tanks No. 919 and No. 920 because of a typo in the permit number.

- On April 21, 1995, DEQ issued a PTC to Chevron for the addition of the diesel storage tanks
   No. 919 and No. 920 to enforce 40 CFR 60, Subpart Kb.
- On June 12, 1995, DEQ received an application from Chevron for a Tier I operating permit.
- On November 23, 1998, DEQ received an updated version of the June 12, 1995 Tier I application.
- On April 2, 2001, DEQ received an application from Chevron for a Tier II operating permit.
- On August 15, 2001, DEQ received an notice of proposed throughput increase from Chevron.
- On December 5, 2001, DEQ received an addendum to the August 15, 2001 request for an increase in product throughput.
- On May 31, 2002, the Tier II application was declared complete.
- On August 16, 2002, DEQ issued a draft Tier II/PTC for facility review.
- On September 6, 2002, DEQ received comments from the Chevron Pipeline Company.
- A public comment period was held between October 31, 2002 and November 29, 2002.
   Comments were received by DEQ. The DEQ's response to the comments is presented in Appendix A.

#### DISCUSSION

#### 1. Emission Estimates

The Chevron Pocatello facility includes the emission sources described below.

Loading Losses/Vapor Destruction Unit: Loading losses are the primary source of evaporative emissions from the loading rack operations. The losses occur as organic vapors in empty cargo tanks are displaced to the atmosphere by the liquid being loaded into the tanks. The loading racks are bottom-loading with a vapor containment and destruction system. Recovered vapors are sent to the VDU.

Emissions from the vapor collection system are controlled by a John Zink vapor destruction unit described as a "vertical cylindrical combustion chamber with refractory insulation and steel inner-lining." The starting sequence begins with a pre-purge in which the air blower purges the combustion chamber for several minutes to remove any residual hydrocarbons. The pilot light then comes on and vapors are fed to the burner through a detonation arrestor by a vapor blower.

The VDU does not appear to meet the definition of a thermal oxidizer since the combustion chamber does not have a specified retention time. This emissions control device meets the definition of a flame.

John Zink, the manufacturer of the VDU, guarantees that the VOC emissions from the unit will not exceed 10 mg VOC/L gasoline loaded (0.000083 lb VOC/gal gasoline). The manufacturer also guarantees that CO emissions will not exceed 10 mg CO/L, and NO<sub>x</sub> emissions will not exceed 4 mg NO<sub>x</sub>/L. According to the Gasoline Distribution MACT 2001 Annual Pocatello Report (January 28, 2001), the performance test for the VDU demonstrated VOC emissions less than 10 mg VOC/L gasoline confirming the manufactures specifications.

The vapor destruction unit will operate while diesel and transmix is loaded. However, the emissions from these two fuel types is nearly zero when uncontrolled; therefore, Chevron calculated VDU emissions of VOC from the diesel and transmix loading racks using AP-42 equations. A summary of emissions from the VDU is presented in Table 1.

Table 1. Emissions Estimates - Va	por Destruction Unit
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PRODUCT	PERMITTED: THROUGHPUT (gal/yr)	VOC EMISSIONS (T/yr)	CO EMISSIONS! (T/yt)	NO. EMISSIONS
Gasoline	370,800,990	15.5	15.5	6.2
Transmix	2,520,000	0.039	0.11	0.042
Diesel	191,453,010	1.3	8.0	3.2
Facility Totals	Not Applicable	16.8	23.6	9.4

Fixed Roof Storage Tanks: There are 23 fixed roof storage tanks that contain refined petroleum products, fuel additives, and/or contaminated water (transmix). The working capacity of these tanks ranges in size from 24 barrels to 19,344 barrels (one barrel equals 42 gallons). Eight of the tanks are vertical and contain diesel fuel, transmix, or gasoline additive. The remaining smaller tanks are horizontal and contain various fuel additives or transmix. Emissions of VOC from fixed roof storage tanks vary as a function of vapor pressure of the stored liquid, tank utilization rate, tank capacity and dimensions, tank color, and atmospheric conditions at the tank location. The VOC emissions from the fixed roof tanks result from liquid evaporation during storage and from changes in the liquid level. Evaporation losses occurring during filling and emptying operations are known as working losses. Losses occurring during standing storage are known as breathing losses. Emissions from the fixed roof storage tanks were calculated using EPA AP-42 equations. The results of Chevron's analysis using AP-42 equations are presented in Appendix B. These calculations were reviewed by DEQ staff and found consistent with DEQ methods.

Floating Roof Storage Tanks: There are 14 floating roof storage tanks that contain refined petroleum products. The working capacity of these tanks ranges in size from 7,380 barrels to 20,000 barrels. All the tanks are vertical and contain either gasoline or diesel fuel. Emissions of VOC from fixed roof storage tanks vary as a function of vapor pressure of the stored liquid, tank utilization rate, tank capacity and dimensions, tank color, and atmospheric conditions and average wind speed at the tank location. Emissions from the floating roof tanks were calculated using EPA AP-42 equations. The results of Chevron's analysis using AP-42 equations are presented in Appendix B. These calculations were reviewed by DEQ staff and found consistent with DEQ methods.

Fugitive Emissions Sources: Fugitive emissions sources at marketing terminals and Pipeline facilities are generally defined as VOC emissions sources not associated with a specific process, but scattered throughout the facility. These sources include storage tanks, valves of all types, flanges, and pump and compressor seals. The EPA has provided interim average emissions factors to estimate most fugitive VOC emissions from various pieces of equipment at marketing terminals. Average emissions factors do not require individual screening values for each component. All that is needed is the number of components in each source category. The number of components in each category is multiplied by the appropriate average emissions factor. The resulting mass for each category can then be added to determine the total fugitive emissions from the facility. The results of Chevron's analysis using EPA fugitive emissions factors are presented in Appendix B. These calculations were reviewed by DEQ staff and found consistent with DEQ methods.

Facility-wide Emissions Summary: Based on the analysis using AP-42 equations, the standing and working VOC emissions from the fixed roof tanks are 0.95 T/yr. The standing and working VOC emissions from floating roof tanks are 23.7 T/yr. These emissions were calculated at the

permitted throughput rates. Emissions from fugitive sources are estimated at 0.89 T/yr, and emissions from maintenance activities are also estimated at 0.89 T/vr.. When summed with the loading losses. VOC emissions estimates submitted by Chevron for the loading racks and storage tanks summed up to 42.3 T/yr. As these emissions are well below the 100 T/yr threshold for major sources, the permitted emissions of the loading racks and storage tanks were multiplied by 120% to account for cyclic fluctuations in the system. The permitted VOC emissions equals 51.8 T/yr. The permitted emissions limits for each source are located in Appendix A of the permit.

HAP Emissions: The aggregate HAP emissions estimates submitted by Chevron for the loading racks and storage tanks summed up to be 1.45 T/yr. The aggregated HAP emissions are 17.2 times smaller than the 25 T/yr aggregate HAP major source threshold. The largest single HAP emission is toluene at 0.51 T/yr. The toluene emissions are 19.6 times smaller than the 10 T/yr single HAP major source threshold. The results of Chevron's HAP emissions analysis are presented in Appendix C. These calculations were reviewed by DEQ staff and found consistent with DEQ methods. Table 2 details the HAPs emissions inventory for the Chevron Pocatello facility.

POTENTIAL HAP	HAPS EMISSIONS (T/YR)
· separation of the second	The state of the s
Acetaldehyde	8.3E-06
Acrolein	3.1E-06
Formaldehyde	9.7E-06
Benzene	1.4E-01
Biphenyl	1.0E-04
Cresols/Cresylic Acid	3.1E-04
Cumene	5.8E-03
Ethyl Benzene	2.0E-02
Hexane	3.0E-01
Methyl tert butyl ether	2.4E-01
Naphthalene	1.5E-03
Phenol	5.7E-04
Styrene	9.5E-04
Toluene	5.1E-01
Xylenes	2.3E-01
TOTAL	1.45

**Table 2 - HAPS EMISSIONS INVENTORY** 

The HAPs listed in Table 1 are defined as VOCs. Therefore, HAP emissions are inherently limited by VOC emissions. Both VOC and HAP emissions are subsequently limited by the facility throughput limitations. The VOC and HAP emissions estimates submitted in the Tier II operating permit application would be exceeded only if Chevron violated the permittee throughput limits.

#### 2. Throughput

The permitted throughput for each fuel product is located in Appendix A of the permit. These are the throughputs and fuel product types requested by Chevron, which allows them to be designated a minor source.

#### 3. 40 CFR 60, Subpart XX

Since the VDU is not a modification or a reconstruction of the loading racks, Chevron is not subject to the provisions of this subpart.

Emissions rates before maintenance factors were applied (Chevron's addendum to the Tier II application received December 11, 2001).

#### 4. 40 CFR 60, Subpart Kb

Tank No. 920 is subject to the provisions of this subpart because it:

- was constructed after July 23, 1984,
- has a capacity greater than 40 m<sup>3</sup>.
- stores a liquid with vapor pressures greater than 5.2 kPa but less than 76.6 kPa, and
- the facility has a gasoline throughput greater than 75,700 L/day.

Tank No. 919 is not subject to this subpart because it stores a liquid that has a vapor pressure less than 3.5 kPa.

Per a telephone message received May 1, 2002, Jim Robbins noted that tank No. 917 had the bottom replaced approximately three years ago. According to the definition of modification, a repair or replacement shall not be considered a physical change. Therefore, Tank No. 917 is not subject to this subpart.

#### 40 CFR 63, Subpart R

On September 9, 2000, the EPA determined that 40 CFR 63, Subpart R applied to Chevron's tank farm in Pocatello, Idaho. According to the memorandum from John S. Seitz, Director of the Office of Air Quality Planning and Standards, "Potential to Emit for MACT Standards – Guidance on Timing Issues", once a MACT standard applies to a facility, the facility must always comply with the MACT standard.

#### 6. Previous Permits To Construct

As discussed in the summary of events, three PTCs were previously issued to the facility. The subjects of all three PTCs were Tanks 919 and 920. Each subsequent PTC superseded the previous PTC; therefore, only the most recent PTC (issued on April 21, 1995) was incorporated into this Tier II/PTC.

Permit Condition 2 of the PTC issued on April 21, 1995 established limits on VOC emissions from the two tanks, and Permit Condition 3.1 established limits product throughput of the tanks. The PTC established VOC emissions on an hourly basis and an annual basis for these two tanks. This Tier II/PTC limits VOC emissions and product throughput on a facility-wide basis; therefore, Permit Conditions 2 and 3.1 of the April 21, 1995 PTC were not incorporated into this permit.

Permit Conditions 3.2, 4.2, 4.3, 5.2, and 5.3 of the PTC issued on April 21, 1995 incorporated the New Source Performance Standards of 40 CFR Part 60, Subpart Kb. The requirements of Subpart Kb are included in the proposed Tier II/PTC permit; therefore, Permit Conditions 3.2, 4.2, 4.3, 5.2, and 5.3 of the PTC issued on April 21, 1995 were not included in the proposed Tier II/PTC permit.

#### Modeling

Modeling was not required for this project.

#### 8. Area Classification

The Chevron Pocatello facility is located in Power County, Idaho, AQCR 61, Zone 12. Power County is classified as a moderate nonattainment area for PM<sub>10</sub>. The area is designated as unclassifiable for all other criteria air pollutants (i.e., CO, NO<sub>x</sub>, SO<sub>x</sub>, and VOCs).

#### 9. Facility Classification

The facility is not a designated facility as defined by IDAPA 16.01.01.006.25 of the *Rules*. The facility is classified as an SM source due to permitted VOC emissions limits below 100 T/yr, and permitted HAP emissions below 10 T/yr single HAP and 25 T/yr aggregated HAP major source thresholds.

#### 10. Regulatory Review

This operating permit is subject to the following permitting requirements:

a.	IDAPA 58.01.01.006 & 7	Definitions
b.	IDAPA 58.01.01.130-136	Excess Emissions
C.	IDAPA 58.01.01.401	Tier II Operating Permit
d.	IDAPA 58.01.01.403	Permit Requirements for Tier II Sources
e.	IDAPA 58.01.01.404.01	Opportunity for Public Comment
f.	IDAPA 58.01.01.404.01(c)(v)	Consideration of Comments and Final Action
g.	IDAPA 58.01.01.404.04	Authority to Revise or Renew Operating Permits
ĥ.	IDAPA.58.01.01.405	Conditions for Tier II Operating permits
i.	IDAPA 58.01.01.406	Obligation to Comply
j.	IDAPA 58.01.01.470	Permit Application Fees for Tier II Permits
k.	IDAPA 58.01.01.625	Visible Emissions
1.	IDAPA 58.01.01.650-651	General Rules for the Control of Fugitive Dust
m.	IDAPA 58.01.01.728	Sulfur Content Limit for Distillate Fuel Oil
n.	Section 37-2506,Idaho Code	Quality Standards for Motor Gasoline and Distillate Fuel Oil-
		Specifications Set By American Society of Testing and Materials
O.	40 CFR 60, Subpart Kb	Standards of Performance for VOC Storage Vessels
p.	40 CFR 60, Subpart XX	Standards of Performance for Bulk Gasoline Terminals
q.	40 CFR 63, Subpart R	Emission Standards for Gasoline Facilities
		•

#### **AIRS**

#### AIRS/AFS FACILITY-WIDE CLASSIFICATION DATA ENTRY FORM

AIR PROGRAM	SIP	PSD	NSPS (Part	NESHAP (Part 61)	MACT (Part 63)	TITLE V	AREA CLASSIFICATION  A Attainments
POLLUTANT 2	ay a		60)2 5				© U– Unclassifiable ■ N–Nonattainment
SO <sub>2</sub>	В						U
NO <sub>x</sub>	В						U
СО	В						U
PM <sub>10</sub>	В			:			N
PT (Particulate)	В						U
VOC	SM		SM			SM	U
THAP (Total HAPs)	В				8	3	<del>-</del>
			APP	LICABLE SUB	PART		
			Kb		R		

#### AIRS/AFS Classification Codes:

- A = Actual or potential emissions of a pollutant are above the applicable major source threshold. For NESHAP only, class "A" is applied to each pollutant, which is below the 10 (T/yr threshold, but which contributes to a plant total in excess of 25 T/yr of all NESHAP pollutants.
- SM = Potential emissions fall below applicable major source thresholds if and only if the source complies with federally enforceable regulations or limitations.
- B = Actual and potential emissions below all applicable major source thresholds.
- C = Class is unknown.
- ND = Major source thresholds are not defined (e.g., radionuclides).

#### **FEES**

This permit is for a synthetic minor permit, therefore, the facility is exempt from paying the Tier II processing fee in accordance with IDAPA 58.01.01.407.02.d. The facility is current with the Registration and Registration Fees in accordance with IDAPA 58.01.01.525.

#### RECOMMENDATIONS

Based on the review of the application materials, and all applicable state and federal regulations, staff recommends that DEQ issue a final Tier II operating permit and Permit to Construct to the Chevron Pipeline Company in Pocatello, Idaho. An opportunity for public comment on the air quality aspects of the proposed operating permit have been provided in accordance with IDAPA 58.01.01.404.01.c.

MJS/MS:sm G:\Air Quality\Stationary Source\Ss Ltd\T2\Nw Terminalling Pocatello\Final Prep\T2-9506-099-1 Tech Memo.Doc

cc: Tiffany Floyd, Pocatello Regional Office

#### APPENDIX A

**Response To Public Comments** 

#### January 22, 2003

# STATE OF IDAHO DEPARTMENT OF ENVIRONMENTAL QUALITY RESPONSE TO PUBLIC COMMENTS ON DRAFT AIR QUALITY TIER II OPERATING PERMIT/PERMIT TO CONSTRUCT FOR CHEVRON PIPELINE CO. AND NORTHWEST TERMINALLING COMPANY POCATELLO TERMINAL LOCATED IN POCATELLO, IDAHO

#### Introduction

As required by IDAPA 58.01.01.404 (*Rules for the Control of Air Pollution in Idaho*), the Department of Environmental Quality (Department) provided for public comment the Chevron Pipeline Co. and Northwest Terminalling Company draft Tier II operating permit/Permit to Construct. Public comment packages, which included the application materials, draft permit, and technical memorandum, were made available for public review at the Marshall Public Library in Pocatello, the Departments Pocatello Regional Office, and the Departments State Office in Boise. The public comment period was held from October 31, 2002 to November 29, 2002. Comments regarding the air quality aspects of the draft permit are provided below with the Departments response immediately following. A final permit that incorporates the public comments has been crafted and will be issued by the Department.

#### **Public Comments and Department Responses**

Comment 1: We would prefer having the CFR regulations referenced rather than copied verbatim into the permit. The permit is rather voluminous, and therefore, not very user friendly.

The Department included the CFR regulations verbatim at the request of Department inspectors. Department inspectors prefer to have the applicable portions of CFR regulations within the permit to assist with facility inspections by alleviating uncertainty in the field as to what portion of CFR regulations apply to an emissions unit.

Comment 2: "Regulated Sources" Section, permit page 5 – At the Pocatello facility, there is not a DRA tank as noted in the table. Delete this item from the table.

The reference to the DRA tank has been removed from the table on page 5 of the permit.

Comment 3: Permit Condition 2.13 – The reference to "ASTM Grade 4, 5, and 6 residual fuel" was not included in previous (August 16, 2001) versions of the draft permit. Additionally, these grades fuel are not located at the facility.

Permit Condition 2.13 is within the facility-wide permit conditions. These conditions are standard conditions included in every permit. The Department's omission of the residual oil sulfur content standard in the permit was an oversight that was corrected in the proposed permit. In accordance with Permit Condition 2.14, the permittee is required to monitor sulfur content of any shipment of distillate oil or residual oil received at the facility. If the facility does not receive residual oil, no monitoring or recordkeeping is necessary.

Comment 4: There were several comments regarding calculating VOC emissions on a monthly and 12-month rolling basis (Permit Conditions 3.3, 3.7, 4.2, and 4.6).

The Department has removed the requirement for calculating VOC emissions on a monthly basis. The Tier II/PTC is being issued to limit the facility's potential to emit (PTE) to below major source thresholds. To calculate emissions, the permittee used the *Tanks* program and specified throughput

rates. Therefore, if the permittee monitors throughput rates, and the throughput rates are below the rates modeled in Tanks, then the permittee is reasonably assured of complying with the annual VOC emissions limits. The permittee is required to monitor throughput rates, but is not required to calculate emissions on a 12-month rolling basis.

Comment 5:— There were several comments regarding calculating product throughput rates on a monthly and 12-month rolling basis (Permit Conditions 3.4, 3.6, 4.3, 4.5.1). The permittee requests the throughput rates be calculated once per calendar year.

As discussed in the response to Comment 4, the permittee is required to monitor product throughput rates to reasonably assure compliance with the annual VOC emissions limits in the permit.

Attachment A is an Environmental Protection Agency (EPA) documentation regarding appropriate time frames for limiting PTE. Please note Sections I - IV of the guidance, as these discussions specifically address time frames. EPA recommends production or operational limits intended to reduce potential to emit be as short-term as possible and should generally not exceed one month. In cases where it is not reasonable to hold a source to a one-month limit, "...a limit spanning a longer time is appropriate if it is a rolling limit."

In developing the permit, the Department limited the PTE of VOC emissions from the storage tanks to below major facility thresholds. The emission limit is an annual standard. In accordance with EPA guidance, the emission limit, operational limit, and associated monitoring requirements must be based on a rolling 12-month time frame in order to be enforceable.

Comment 6: Permit Condition 3.5 – It is unclear of the intent of "procedures shall be logged". Currently the facility has an operating procedure for truck drivers who load at the facility. We believe that this fulfills the intent of this condition.

The Department agrees that the operating procedure fulfills the intent of the permit condition. The permit condition was reworded to state, "Operating procedures for the loading rack shall be maintained at the facility and be made available to Department representatives upon request."

Comment 7: Appendix B, page 37 & Facility-wide Emissions Summary – Change 50.8 tons per year to 51.8 tons per year.

Maintenance activities contributing 1-ton per year of VOC emissions were not accounted for in the emission inventory. The Department added these emissions to the inventory. The additional emissions will not cause annual VOC emissions from the facility to exceed the major source threshold.

The following comments were submitted and address typographical errors within the permit or errors in process descriptions. The suggested corrections to the errors were made within the permit and/or technical memorandum.

- Permit Condition 2.14 Change reference "specified on Permit Condition 2.14" to "specified on Permit Condition 2.13".
- Permit Condition 3.1 Change "The loading racks are bottom loading racks" to "The loading rack is a bottom loading rack with a vapor...".
- Permit Condition 3.2 Change "...they are combined with natural gas and..." to "...where they are
  destroyed...". The combustor does not use natural gas to assist the destruction process.
- Permit Condition 3.3 Change "...loading racks..." to "...loading rack...".

**END OF COMMENTS** 

#### ATTACHMENT A

# UNITED STATES ENVIRONMENTAL PROTECTION AGENCY Washington, D.C. 20460

#### JUN 13 1989

#### **MEMORANDUM**

SUBJECT: Guidance on Limiting Potential to Emit in New Source Permitting

FROM: Terrell E. Hunt

Associate Enforcement Counsel

Air Enforcement Division

Office of Enforcement and Compliance Monitoring

John S. Seitz, Director

Stationary Source Compliance Division
Office of Air Quality Planning and Standards

TO: Addressees

This memorandum transmits the final guidance on conditions in construction permits which can legally limit a source's potential to emit to minor or de minimis levels. We received many helpful comments on the January 24, 1989 draft of this guidance, and have incorporated the comments into the final document wherever possible. A summary of the major changes which have been made to the guidance in response to these comments is provided below.

Several commenters noted that the draft guidance used the term "federally enforceable" to mean both federally enforceable as defined in the new source regulations (40 C.F.R. Sections 52.21(b) (17), 51.165(a) (1) (xiv), 51.166(b) (17)), and enforceable as a practical matter. We have tried to distinguish the places where each term should be used, explained the relationship between the two terms, and indicated that in order to properly restrict potential to emit, limitations must be both federally enforceable as defined in the regulations and practically enforceable.

Some commenters requested that the section on averaging times for production limits be more specific as to when it is appropriate to use limitations which exceed a one month time basis. We have tried to explain why it is not possible to develop generic criteria for making this distinction, and to indicate situations where exceptions to the policy that production and operation limitations not exceed one month may be warranted.

There were some requests for a section on enforcement. We have included a new Section VI which addresses this topic. We also received many good suggestions on the example permit limitations. The section on examples has been substantially reworked to reflect your comments.

Finally, we learned through the comments that in two specific circumstances, short term emission limits are the most useful and reasonable way to restrict and verify limits on potential to emit. These circumstances are: 1) when control equipment is installed but control equipment operating parameters are difficult to measure during enforcement inspections; and 2) in surface coating operations with numerous and unpredictable use of coatings containing varying VOC content, where add-on control equipment is not employed. Therefore, we have made a narrow exception to the flat prohibition on use of emission limits to restrict potential to emit for these specific circumstances, and only when certain additional conditions have been met.

Again, we appreciate the thoughtful comments we have received on this guidance. Please insert this document into your Clean Air Act Compliance/Enforcement Policy Compendium as Item Number H.3. If you have any questions, please contact Judith Katz in the Air Enforcement Division at FTS 382-2843, or Sally Farrell in the Stationary Source Compliance Division at FTS 382-2875.

#### Addressees:

Regional Counsels Regions I-X

Regional Counsel Air Branch Chiefs Regions I-X

Air Management Division Directors Regions I, III, and IX

Air and Waste Management Division Director Region II

Air, Pesticides, and Toxics Management Division Directors Regions IV and VI

Air and Radiation Division Director Region V

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**Environmental Enforcement Section** 

DOJ

LIMITING POTENTIAL TO EMIT IN NEW SOURCE PERMITTING

JUNE 13, 1989

# AIR ENFORCEMENT DIVISION OFFICE OF ENFORCEMENT AND COMPLIANCE MONITORING

STATIONARY SOURCE COMPLIANCE DIVISION OFFICE OF AIR QUALITY PLANNING AND STANDARDS

#### Limiting Potential to Emit in New Source Permitting

- I. Introduction
- II. The Louisiana-Pacific Case
- III. Types of Limitations that will Limit Potential to Emit
- IV. Time Periods for Limiting Production and Operation
- V. Sham Operational Limits
  - A. Permits with conditions that do not reflect a source's planned mode of operation are void ab initio and cannot act to shield the source from the requirement to undergo preconstruction review.
    - 1. Sham permits are not allowed by 40 CFR 52.21(r) (4)
    - 2. Sham permits are not allowed by the definition of potential to emit: 40 CFR 52.21(b) (4), 51.165(a) (1) (iii), 51.166(b) (4)
    - 3. Sham permits are not allowed by the Clean Air Act
  - B. Guidelines for determining when minor source construction permits are shams.
    - 1. Filing a PSD or nonattainment NSR application
    - 2. Applications for funding
    - 3. Reports on consumer demand and projected productions levels
    - 4. Statements of authorized representatives of the source regarding plans for operation
- VI. Enforcement Procedures
- VII. Examples
- VIII. Conclusion

#### Limiting Potential to Emit in New Source Permitting

#### I. Introduction

Whether a new source or modification is major and subject to new source review under Parts C and D of the Clean Air Act is dependent on whether that source or modification has or will have the potential to emit major or significant amounts of a regulated pollutant. Therefore, the definition of "potential to emit" under the new source regulations is extremely important in determining the applicability of new source review to a particular source. The federal regulations define "potential to emit" as:

the maximum capacity of a stationary source to emit a pollutant under its physical and operational design. Any physical or operational limitation on the capacity of the source to emit a pollutant, including air pollution control equipment and restrictions on hours of operation or on the type or amount of fuel combusted, stored or processed, shall be treated as part of its design if the limitation or the effect it would have on emissions is federally enforceable.

40 C.F.R Sections 52.21(b) (4), 51.165(a) (1) (iii), 51.166(b) (4).

Permit limitations are very significant in determining whether a source is subject to major new source review. This is because they are the easiest and most common way for a source to obtain restrictions on its potential to emit. A permit does not

have to be a major source permit to legally restrict potential emissions. A minor source construction permit issued pursuant to a state program approved by EPA as meeting the requirements of 40 C.F.R. Section 51.160 is federally enforceable. In fact, any permit limitation can legally restrict potential to emit if it meets two criteria: 1) it is federally enforceable as defined by 40 C.F.R. Sections 52.21(b) (17), 51.165(a) (1) (xiv), 51.166(b) (17), i.e., contained in a permit issued pursuant to an EPA-approved permitting program or a permit directly issued by EPA, or has been submitted to EPA as a revision to a State Implementation Plan and approved as such by EPA; and 2) it is enforceable as a practical matter. The second criterion is an implied requirement of the first criterion. A permit requirement may purport to be federally enforceable, but, in reality cannot be federally enforceable if it cannot be enforced as a practical matter.

Non-permit limitations can also legally restrict potential to emit. These limitations include

New Source Performance Standards codified at 40 C.F.R. Part 60 and National Emission

Standards for Hazardous Air Pollutants codified at 40 C.F.R. Part 61.

The appropriate means of restricting potential to emit through permit conditions has been an issue in recent enforcement cases. Through these cases and through guidance issued by EPA, the Agency has addressed three questions: what types of permit

limitations can legally limit potential to emit; whether long averaging times for production limitations are enforceable as a practical matter; and whether sources may limit potential to emit to minor source levels as a means of circumventing the preconstruction review requirements of major source review.

#### II. The Louisiana-Pacific Case

In <u>United States v. Louisiana-Pacific Corporation</u>, 682 F. Supp. 1122 (D. Colo. Oct. 30, 1987) and 682 F. Supp. 1141 (D. Colo. March 22, 1988), Judge Alfred Arraj discussed the type of permit restrictions which can be used to limit a source's potential to emit. The Judge concluded that:

... not all federally enforceable restrictions are properly considered in the calculation of a source's potential to emit. While restrictions on hours of operation and on the amount of materials combusted or produced are properly included, blanket restrictions on actual emissions are not.

#### 682 F. Supp. at 1133.

The Court held that Louisiana-Pacific's permit conditions which limited carbon monoxide emissions to 78 tons per year and volatile organic compounds to 101.5 tons per year should not be considered in determining "potential to emit" because these blanket emission limits did not reflect the type of permit conditions which restricted operations or production such as limits on hours of operation, fuel consumption, or final product.

The Louisiana-Pacific court was guided in its reasoning by the D.C. Circuit's holding in Alabama Power v. Costle, 636 F. 2d 323 (D.C. Circuit 1979). Before Alabama Power, EPA regulations required potential to emit to be calculated according to a source's maximum uncontrolled emissions. In Alabama Power, the D. C. Circuit remanded those regulations to EPA with instructions that the Agency include the effect of in-place control equipment in defining potential to emit. EPA went beyond the minimum dictates of the D.C. Circuit in promulgating revised regulations in 1980 to include, in addition to control equipment, any federally enforceable physical or operational limitation. The Louisiana-Pacific court found that blanket limits on emissions did not fit within the concept of proper restrictions on potential to emit as set forth by Alabama Power.

Moreover, Judge Arraj found that:

...a fundamental distinction can be drawn between the federally enforceable limitations which are expressly included in the definition of potential to emit and (emission) limitations.... Restrictions on hours of operation or on the amount of material which may be combusted or produced ... are, relatively speaking, much easier to "federally enforce." Compliance with such conditions could be easily verified through the testimony of officers, all manner of internal correspondence and accounting, purchasing and production records. In contrast, compliance with blanket restrictions on actual emissions would be virtually impossible to verify or enforce.

Id. Thus, Judge Arraj found that blanket emission limits were not enforceable as a practical matter.

Finally, the Court reasoned that allowing blanket emission limitation to restrict potential to emit would violate the intent of Congress in establishing the Prevention of Significant Deterioration (PSD) program.

#### III. Types of Limitations that will Restrict Potential to Emit

As an initial matter in this discussion, a few important terms should be defined. Emission limits are restrictions over a given period of time on the amount of a pollutant which may be emitted from a source into the outside air. Production limits are restrictions on the amount of final product which can be manufactured or otherwise produced at a source. Operational limits are all other restrictions on the manner in which a source is run, including hours of operation, amount of raw material consumed, fuel combusted, or conditions which specify that the source must install and maintain add-on controls that operate at a specified emission rate or efficiency. All production and operational limits except for hours of operation are limits on a source's capacity utilization. Potential emissions are defined as the product of a source's emission rate at maximum operating capacity, capacity utilization, and hours of operation.

To appropriately limit potential to emit consistent with the opinion in <u>Louisiana-Pacific</u>, all permits issued pursuant to 40 C.F.R. Sections 51.160, 51.166, 52.21 and 51.165 must contain a

production or operational limitation in addition to the emission limitation in cases where the emission limitation does not reflect the maximum emissions of the source operating at full design capacity without pollution control equipment. Restrictions on production or operation that will limit potential to emit include limitations on quantities of raw materials consumed, fuel combusted, hours of operation, or conditions which specify that the source must install and maintain controls that reduce emissions to a specified emission rate or to a specified efficiency level. Production and operational limits must be stated as conditions that can be enforced independently of one another. For example, restrictions on fuel which relates to both type and amount of fuel combusted should state each as an independent condition in the permit. This is necessary for purposes of practical enforcement so that, if one of the conditions is found to be difficult to monitor for any reason, the other may still be enforced.

When permits contain production or operational limits, they should also have recordkeeping requirements that allow a permitting agency to verify a source's compliance with its limits. For example, permits with limits on hours of operation or amount of final product should require an operating log to be kept in which the hours of operation and the amount of final product produced are recorded. These logs should be available

for inspection should staff of a permitting agency wish to check a source's compliance with the terms of its permit.

When permits require add-on controls operated at a specified efficiency level, permit writers should include, so that the operating efficiency condition is enforceable as a practical matter, those operating parameters and assumptions which the permitting agency depended upon to determine that the control equipment would have a given efficiency.

An emission limitation alone would limit potential to emit only when it reflects the absolute maximum that the source could emit without controls or other operational restrictions. When a permit contains no limits on capacity utilization or hours of operation, the potential to emit calculation should assume operation at maximum design or achievable capacity (whichever is higher) and continuous operation (8760 hours per year).

The particular circumstances of some individual sources make it difficult to state operating parameters for control equipment limits in a manner that is easily enforceable as a practical matter. Therefore, there are two exceptions to the absolute prohibition on using blanket emission limits to restrict potential to emit. If the permitting agency determines that setting operating parameters for control equipment is infeasible in a particular situation, a federally enforceable permit

containing short term emission limits (e.g. lbs per hour) would be sufficient to limit potential to emit, provided that such limits reflect the operation of the control equipment, and the permit includes requirements to install, maintain, and operate a continuous emission monitoring (CEM) system and to retain CEM data, and specifies that CEM data may be used to determine compliance with the emission limit.

Likewise, for volatile organic compound (VOC) surface coating operations where no add-on control is employed but emissions are restricted through limiting VOC contents and quantities of coatings used, emission limits may be used to restrict potential to emit under the following limited circumstances. If the permitting agency determines for a particular surface coating operation that operating and production parameters (e.g. gallons of coating, quantities produced) are not readily limited due to the wide variety of coatings and products and due to the unpredictable nature of the operation, emission limits coupled with a requirement to calculate daily emissions may be used to restrict potential to emit. The source must be required to keep the records necessary for this calculation, including daily quantities and the VOC content of each coating used. Emission limits may be used in this limited circumstance to restrict potential to emit since, in this case, emission limits are more easily enforceable than operating or production limits.

IV. Time Periods For Limiting Production and Operation.

As discussed above, a limitation specifically recognized by the regulations as reducing potential to emit is a limitation on production or operation. However, for these limitations to be enforceable as a practical matter, the time over which they extend should be as short term as possible and should generally not exceed one month. This policy was explained in a March 13, 1987 memorandum from John Seitz to Bruce Miller, Region IV. The requirement for a monthly limit prevents the enforcing agency from having to wait for long periods of time to establish a continuing violation before initiating an enforcement action.

EPA recognizes that in some rare situations, it is not reasonable to hold a source to a one month limit. In these cases, a limit spanning a longer time is appropriate if it is a rolling limit.

However, the limit should not exceed an annual limit rolled on a monthly basis. EPA cannot now set out all inclusive categories of sources where a production limit longer than a month will be acceptable because every situation that may arise in the future cannot now be anticipated. However, permits where longer rolling limits are used to restrict production should be issued only to sources with substantial and unpredictable annual variation in production, such as emergency

boilers. Rolling limits could be used as well for sources which shut down or curtail operation during part of a year on a regular seasonal cycle, but the permitting authority should first explore the possibility of imposing a month-by-month limit. For example, if a pulp drier is periodically shut down from December to April, the permit could contain a zero hours of operation limit for each of those months, and then the appropriate hourly operation limit for each of the remaining months. Under no circumstances would a production or operation limit expressed on a calendar year annual basis be considered capable of legally restricting potential to emit.

#### V. Sham Operational Limits

In the past year, several sources have obtained purportedly federally enforceable permits with operating restrictions limiting their potential to emit to minor or de minimis levels for the purpose of allowing them to commence construction prior to receipt of a major source permit. In such cases where EPA can demonstrate an intent to operate the source at major source levels, EPA considers the minor source construction permit void <u>ab initio</u> and will take appropriate enforcement action to prevent the source from constructing or operating without a major source permit.

The following example illustrates the kind of situation addressed in this section: An existing major stationary source proposes to add a 12.5 megawatt electric utility steam generating unit, and applies for a federally enforceable minor source permit which restricts operation at the unit to 240 hours per year. Because the project is designed as a baseload facility, EPA does not believe that the source intends to operate the facility for only 240 hours a year. Further investigation would probably uncover documentation of the source's intent to operate at higher levels than those for which it is permitted.

This situation raises the question of whether a source can lawfully bypass the preconstruction or premodification review requirements of Prevention of Significant Deterioration (PSD) and nonattainment New Source Review by committing to permit conditions which restrict production to a level at which the source does not intend to operate for any extensive time. If, after constructing and commencing operation, the source obtains a relaxation of its original permit conditions prior to exceeding them, does this constitute a violation of the preconstruction review requirements? This section discusses why it is improper to construct a source with a minor source permit when there is intent to operate as a major source, and provides guidelines for identifying these "sham" permits.

A. Permits with conditions that do not reflect a source's planned mode of operation are void ab initio and cannot act to shield the source from the requirement to undergo preconstruction review.

1. Sham permits are not allowed by 40 CFR Section 52.21(r) (4) Section 52.21(r) (4) states:

At such time that a particular source or modification becomes a major stationary source or major modification solely by virtue of a relaxation in any enforceable limitation which was established after August 7, 1980 on the capacity of the source or modification otherwise to emit a pollutant, such as a restriction on hours of operation, then (PSD) shall apply to the source or modification as though construction had not yet commenced on the source or modification.

When a source that is minor because of operating restrictions in a construction permit later applies for a relaxation of that construction permit which would make the source major, Section 52.21(r) (4) prescribes the methodology for determining best available control technology (BACT). However, it does not foreclose EPA's ability, in addition to the retroactive application of BACT and other requirements of the PSD program, to pursue enforcement where the Agency believes that the initial minor source permit was a sham. EPA will limit its activity to requiring application of 40 CFR 52.21(r) (4) only for the cases where a source legitimately changes a project after finding that the operating restrictions which were taken in good faith cannot be complied with. Whether a source has acted in good faith is a factual question which is answered by available evidence in the particular case.

2. Sham permits are not allowed by the definition of potential to emit:

40 C.F.R. Sections 52.21(b) (4), 51.165(a) (1) (iii), 51.166(b) (4).

The definition of potential to emit enables sources to obtain federally enforceable permits with operational restrictions as a means of limiting emissions to minor source levels. However, implicit in the application of these limitations is the understanding that they comport with the true design and intended operation of the project.

3. Sham permits are not allowed by the Clean Air Act

Parts C and D of the Clean Air Act exhibit Congress's clear intent that new major sources of air pollution be subject to <u>preconstruction</u> review. The purposes for these programs cannot be served without this essential element. Therefore, attempts to expedite construction by securing minor source status through the receipt of operational restrictions from which the source intends to free itself shortly after operation are to be treated as circumvention of the preconstruction review requirements.

B. Guidelines for determining when minor source construction permits are shams.

EPA's determination that a purportedly federally enforceable construction permit is a sham is made based on an evaluation of specific facts and evidence in each individual case. The following are criteria which should be scrutinized when making such a determination:

#### 1. Filing a PSD or nonattainment NSR permit application

If a major source or major modification permit application is filed simultaneously with or at approximately the same time as the minor source construction permit, this is strong evidence of an intent to circumvent the requirements of preconstruction review. Even a major source application filed after the minor source application, but either before operation has commenced or after less than a year of operation should be looked at closely.

#### 2. Applications for funding

Applications for commercial loans or, for public utilities, bond issues, should be scrutinized to see if the source has guaranteed a c ertain level of operation which is higher than that in its construction permit. If the project would not be funded or if it would not be economically viable if operated on an extended basis

In such cases, the entire source must still go through new source review, during which, for PSD review, all pollutants for which there is a net significant increase must be analyzed for BACT. In nonattainment new source review, new sources must have LAER determinations only for pollutants for which they are major. Major modifications, however, must have LAER determinations for all nonattainment pollutants emitted in significant amounts. If the valid limits in a partially void minor source construction permit keep certain pollutants below significance levels, then those pollutants would not have to be analyzed for BACT or LAER. However, if a source or modification is determined to be major for PSD or NSR because part of its minor permit is deemed void, it would have to undergo BACT or LAER analysis for all significant pollutants.

#### VI. Enforcement Procedures

This guidance has discussed permit conditions which will legally restrict potential to emit, shielding a source from the requirement to comply with major new source permitting regulation. Failure by a permitting agency to adhere to these guidelines may result in a permit that does not legally restrict potential to emit, thereby subjecting a source to major new source review. If that source has not gone through preconstruction review, it is a significant violator of the Clean Air Act and is subject to enforcement for constructing or

(at least a year) at the permitted level of production, this should be considered as evidence of circumvention.

3. Reports on consumer demand and projected production levels.

Stockholder reports, reports to the Securities and Exchange Commission, utility board reports, or business permit applications should be reviewed for projected operation or production levels. Ifreported levels are necessary to meet projected consumer demand but are higher than permitted levels, this is additional evidence of circumvention.

4. Statements of authorized representatives of the source regarding plans for operation.

Statements by representatives of the source to EPA or to state or local permitting agencies about the source's plans for operation can be evidence to show intent to circumvent preconstruction review requirements.

Note that if a determination is made that a permit is a "sham" for one pollutant and, therefore, the source is a major source or major modification, the permit may possibly still contain valid limits on potential to emit for other pollutants.

modifying without a major new source permit.

The enforcement options available to EPA in these situations include administrative action under Sections 167 or 113 (a) (5) of the Act or federal judicial action under Sections 113 (b) (2), 113 (b) (5), 113(c), or 167. Which enforcement option is selected depends on the facts of the particular situation. (See July 15, 1988 guidance on EPA Procedures for Addressing Deficient New Source Permits.)

#### VII. Examples

The following examples are provided to illustrate the type of permit restrictions which would and would not legally limit potential to emit to less than major source thresholds. These examples are provided for purposes of clarifying the potential to emit and averaging time guidance only. They are not intended to reflect all the permit conditions necessary for a valid permit. Specific test methods, compliance monitoring and recordkeeping and reporting requirements are necessary to make permit limitations enforceable as a practical matter. The use of examples where averaging times are the longest times allowed under EPA policies is not intended to necessarily condone the selection of the longest averaging times; averaging times should in practice be as short as possible.

1. The minor source construction permit for a boiler contains the following restrictions: 250,000 gal fuel/month; 0.8% S fuel; 8000 hours/year.

These conditions are federally enforceable production and operation limits, but do not limit potential to emit because one of them does not meet EPA policies on enforceability as a practical matter. The averaging time for hours of operation, one of the operational limits necessary to restrict emissions to less than 250 tpy, exceeds a monthly or rolling yearly limit. If, instead of 8000 hours/year, the hourly restriction were stated as 666 hours/month, the permit would serve to keep the source a minor source, assuming the permit contains appropriate recordkeeping provisions.

2. A waferboard plant which has the physical capacity to emit over 300 tpy of carbon monoxide in the absence of using specific combustion techniques has the following permit restriction as the sole emission limitation: 249 tpy.

This does not limit potential to emit since an operational or production restriction is necessary for the source to be restricted to 249 tpy. The permit must contain a restriction on hours of operation or capacity utilization which, when multiplied by the maximum emission rate for the CO sources at the plant, results in emissions of 249 tpy. Additionally, while the

emission limit alone cannot restrict potential to emit, the emission limit is unenforceable as a practical matter since it is limited on an annual basis. The permit should contain a short term emission limit (in addition to the annual emission limit), consistent with the compliance period or parameter in the applicable test method for determining compliance.

3. A small scale rock crushing plant that cannot emit more than 240 tpy under maximum operation without controls (including plant-wide particulate emissions from transfer and storage operations) has the following permit restriction as the sole emission limitation: 240 tpy particulate matter.

Since no operational limitations are necessary for the source to emit below 250 tpy, no operational restrictions need be in the permit to limit potential to emit. However, although this is not a major source, the state agency should express the emission limit in this permit as a lb/hour measure or gr/dscf so that it will be enforceable as a practical matter.

4. A plant consisting solely of a small rock crusher has the following permit restrictions:0.05 lb gr PM/dscf; fabric filter must be employed and maintained at 99% efficiency.

Assuming that maintaining the fabric filter at 99% efficiency will result in emissions of less than 250 tpy, this permit would limit

potential to emit if it also contained either 1) parameters that allowed the permitting agency to verify the fabric filter's operating efficiency or 2) a requirement to install and operate continuous opacity monitors (COMs) and a specification that COM data may be used to verify compliance with emission limits. Note that if this second alternative were adopted, it would not be necessary to require that the fabric filter be maintained at 99% efficiency.

To determine potential to emit, the efficiency rate of the fabric filter would be multiplied by the maximum uncontrolled emission rate, the maximum number of operating hours and maximum throughput capacity since there are no other operating or production limits. However, the efficiency rate of the fabric filter would not be enforceable as a practical matter unless there were an enforceable means to monitor ESP performance on a short term basis. The two alternatives mentioned above would satisfy this requirement.

5. A surface coating operation has the capability of utilizing 15,000 gal coating/month, with the following permit restrictions: 3.0 lb VOC/gal coating minus water; 20.5 tons

VOC/month; monthly VOC emissions to be determined from records of the daily volumes of coatings used times the manufacturers specified VOC content.

This does not limit potential to emit since the source has the physical capacity to exceed 250 tpy of VOC, and the permit does not contain a production or an operational limitation. A monthly limit on gallons of coating used which when multiplied by 3.0 lb/gal equates to less than the 250 tpy threshold 13,500 gallons/month), with appropriate recordkeeping, would generally be necessary to limit potential to emit. If, however, the permitting agency determines, due to the wide variety of coatings employed and products produced, that restrictions on operation or production are not practically enforceable, then the above emission limits could restrict potential to emit if there are requirements that the source calculate emissions daily, and keep the appropriate records.

If the source was alternatively to meet the 20.5 ton/month limit by employing add-on controls, the permit would need to contain an operational limit, such as the requirement to install and operate an incinerator at 99% efficiency. A requirement to monitor incinerator efficiency (either directly or indirectly via temperature monitoring for example), and appropriate recordkeeping retirements to verify compliance with each of the permit conditions would also be necessary to make the permit conditions enforceable as a practical matter. Note, however, that in the case where add-on controls are employed, the source may be able to meet a shorter term emission limit than the ton per month figure.

#### VIII. Conclusion

We hope this guidance will help EPA Regions identify sources which have the potential to emit major amounts of an air pollutant which will subject those sources to the requirements of preconstruction new source review. Every source which is subject to these requirements but has not obtained a major new source permit should be seriously considered for enforcement action.

## **APPENDIX B**

**Volatile Organic Compound Emissions Estimates** 

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1-5000		N/A 0.52			N/A	66.0		T N/A	AI/A	0.0193	N/A	N/A	10,0			/A 508.4	508.4	N/A	N/A	658	N/A	N
1711246	95. CAL 25. 1.73	100 Part (18080)				- 60	0.000		<b>以</b>	CH 1989	100 000	a Catendaria	Part and		1.0	N. Barre		74.00	TO W		area e	Track Co.
A = Con	tant la vaca	r pressure equipor	Co. Hold Wilder	LT = To	in losses		1					Tark emis	lone (lone)	year)		<b>∑</b>  LT = L5	+LW			1:		
		olar absorptance		LW = W	orking losse	**			100		Taris	1.5	LW	1.7			w ()57%, L.S				overuses.	
9 * Con:	stant in the v	apor pressure equal	lon .		epor malecu					1244	901	1,35-				e r	MATELLE Travers	i = (daysiye Host tanks, '	ar in sarvic VV w fPlfdid	カイクいがひくび	itueltani	
		Appr pressure equal	ion-		SORE OF BUILD				7		903	1,35				33		ixontal tank				
	(gameler (				Breather ven Breather ven					# W.*	0	1.3€					DI	= SORT(()	L)(D))/0.785	<b>\$</b> }		
		diameter (ft)					ige flakifa ten	noerafsum	100		905	1,3€.	02 f.0E	01 f,1E-		374	Fe	e verticel to		= HS + HL +	HRO	
		rent pressure range or pressure range		FVN = 1	Venor skesu	une at own.	surface terri	perenture:	26		906	1,3€.				<b>3</b> 1		14. = HS	i/2 raofs, H我C			
		or temp. range, (R)		PVX = 1	Vapor press		sirface tem	ger#bure	4.4	100	(i <u>l</u>	1.3€				<b>9</b> 91		Por sign	ne roofs, H	, – v RG = 9.137	#31	
	ruld helght (!				nciel through		١.		2 14		909	1,36			25			RS	5 = D/2			
HR = TI	nk roof helg	ht (ft)			ank siseli sad		•				930	4.2E							m roofs, HF		(FL)	
	Roof outage				ank cone for		moi:				S-530			-03] 4.1E					e = (SR)(RS			
	nk shell hek				codo bullo le: Average lico					- 1 C	e 1-300							or hortzonki (MV)(PVA))		M. w D.O(L)		
	/apor space							• (R)			1-500	0.05	00 3.30	-00 136		<b>13</b>	77 V T	VA = (10*(A	- 18/1C + (E	T.A - 492)5	/9)))) <u>X</u> 14.7/	700)
₹.,	** Vapor space emperation factor TLX = Daily min. floatd surface temperature (R)  TLX = Daily man. Books surface temperature (R)												TOTAL				'n	A = 0.44(T/	AA) + 0.58(1	(B) + 0.007	Q(adptus)(1)	
	- Mark from these providest factor VLX = Tank max Republication (Filis)										100			"				TB = T/	LA + Bjulphu	9-1		
	* Venter vapor saturator factor VV * Vapor space volume (43)										1 4 126	8 <u>8(3</u> 87)				KE = 6	MATV/TLA	+ {{clefter*	/ + (MILEPIS)	reput Minare Land	17	
L = Lery	Length of lank (ft) WV = Vapor density									200	200	Total S		6. W. C.				eiteTV = 0.7 WesiVV = PV		. Crossinia	and it	
LS - St	anding stora	ga losses	·		Culture St.	THE STATE OF	16 2 2 1 TA	1. 7 L		3	·····	SHe D					a	PVY = 1"	(1048 • MA	C+ITLX.	497(5/9))))	X14,787
التسيير	AND THE PERSON NAMED IN	ga hases			THE PERSON NAMED IN		4					emperakre			9.3			777	Y # TI A +	0.25(defte 1	V)	
		ID OTHER RIFO: Intere of all fuels and										erakun (F)						PVN 4	(10*(A - (PV	C+ITLN	492(5/9])))	¥14.7/7
lat we.	WELLER SE SE LEGE	6 be beneated res	AND DESCRIPTION OF THE PERSON	MANAGEME.								erakse (F)			5.9			¥1	N . TLA -	25(dolla 1	<b>v</b> )	
		PARTY OF THE PARTY OF THE							Lar Contract	& www.	PETTERNIA	ne made [	i a conce (i					etaP8 = P8		-		
2) MV1	ar makanı da	r waterhit flatVS in for it	使 接收功 馬	DEST. LUMB	i Militaria	BOOKEN IN	MAS NEA					at family w	-	1 '	th states		v	Bruse 0	T ~ ( ₩ ¥			
2) MV1	ar makanı da	r waterhit flatVS in for it	ione spugge.	constituents	1 101110	process sy	Wer May	~ en 5				ed (mph) * CE	<u> </u>		10.2 100		K\$ = 1	#1 + 0.053f	PVAXHVOI			
2) MV 3) Vap 4) Stov	or molecula e OK and Lo	r weight (MV) is for it w Suffur Diesel # 1 !	ave stricter	constituents						Site ele	valion (N) =	5E		, '	(00 )2.5		K\$ = 1 W = 0,0010	/1 + 0.053( XWVXPVAX	PVAKHKO) OKKNIKO)	j		
2) MV1	or molecula e OK and Lo	r waterhit flatVS in for it	india	constituents						Site etc Average	valion (N) =	SE et present			400 (8		1C\$ = 1 W = 0,001C For tu	#1 + 0.053f	PVAKHVO) OKKONKOP I, KH = (EBI	j	•	

Note: Throughputs are besid on adversive throughputs shown in The # Permit Application, dated April 2, 2001, plus throughputs are besid on adversive throughputs shown in The # Permit Application, dated April 2, 2001, plus throughput increases expected as a result of adding DRA to system, which is expected to increase gasoline by 186,000 gallons and diesel by 32,000 gallons.

······································	Tark	characteristics	Tark	Palni	Pakil	Roof	Tack	····		***************************************			NORTI	WEST TE			₹¥					
1			Color	Shade	Condition	Туре	volume						*********	POGATE: L FIXED RI	LLO TERM		SIN'INIE					
- 1		•		(XMuse,		_ 1	(\$\ta\8)							UPPOATED			SHUNG					
1			Akyminann,	Rott, N/A,		Cone.	1							O-DATE	A-1004. 11	4						
1	AST or	Horizontal or	] belge, gray, red.	prediction, primer, or	gooder	dome,	. !															
Cent 1	USY	Verfical	Or white	opecular	DOXX	er N/A	· •	Conte	rds I	A 1	aigha	8	C	0 1	DE j	de <sup>n</sup> abili	deltaPV	deliaTV	}# <u>[</u>	HR	HRO	H\$
A 100	AST	Vertical	White	N/A	Good	Cone	500	A-16/8		2,351	0.17	163.21	82.4	15.0	N/A	0.08	0,0120	25.9	H_D	0.47	0,15	16,0
A 185	AST	Hotzonial	White	NA	Good	N/A	143	Addit	ve .	2.351	0.17	183,21	62.4	8.0	12.8	0,06	0.0170	25.9	N/A	M/A	NIA	N/A
A102	AST	Horizonial	White	N/A	Good	N/A	95	Addit	we i	2.351 1	0,17	163.21	82,4	8.0	12,1	0.08	0.0120	75.9	N/A	N/A	N/A	NIA
A103	AST	Hortzoreal	White	N/4	Good	N/A	98	Adkti	lve i	2.351	0,17	163,21	62.4	8,0	10,6	0,05	0,0120	25.9	N/A	NIA	N/A	N/A
A104	AŞT	Horizonial	White	NIA	Good	N∤A	98	Addi	Ne i	2.351	0,17	163.21	62.4	8,0	10.6	0.06	0,0120	25,9	NIA	N/A	N/A	NIA
A105	AST	Horizorial	White	A164	Good	N/A	48	<b>A44</b>	ive i	2,351	8,47	163:21	52.4	5.3	9.0	0.06	0.0120	25,9	N/A	NIA	N/A	MIA
A 106	AST	Horizonial	White	NIA	Good	NIA	48	Add	live	2.351	0,17	163,21	62.4	5.3	9.0	0,08	0.0120	25.9	N/A	N/A	N/A	N/A
A107	AST	Horizontal	White	N/A	Good	NIA	74	Arks	tive	2,351	0,17	163,21	62,4	4.0	7,5	0.06	0.0120	75,9	N/A	MA.	N/A	N/A
A105	AST	Horizonfal	White	N/A	Good	N/A	715	Add	live	2,351	0,17	163.21	62.4	0.0	15.6	0,06	0,0120	25.9	N/A	MIA	N/A	NIA
AHY	AST	Horizontal	Ahmins			N/A	95	Add		2,351	9,39	163,21	57.4	7,5	10,7	0.06	0,0178	35.3	N/A	N/A	N/A	NIA
A110	AST	Hortzontal	White	N/A	Good	N/A	95	Add		2.351	0.17	163.21	52.4	7,0	7 11.7	0.06	0,0120	25.9	N/A	N/A	N/A	N/A
A111	AST	Horizontal	White	N/A	Good	N/A	50	Add		2,351	0,17	183,21	<b>82.</b> €	3,6	5.4	0,96	0,0120	25,9	N/A	N/A	N/A	N/A
DFLA	AST	Horizoniai	White	N/A	Good	N/A	37	Đ		2.842	0.17	355.22	99.9	5.0	8.2	0.08	0.0022	25.9	N/A	N/A	N/A	N/A
	n Conference in the State of the Conference in t		The second second second			35.24727		13.5		****			7.7	<b>建筑等等</b>		100-71	2.00	A CONTRACTOR	A 44.0. 4 44.		7.1	100
Tarek	HVO	KE KN	KP	K\$	L_	MV.	N	PBP	VB4	₽VA.	P\#I	₽VX	0	PS	58	76	TLA.	TLN:	TLX	VI.X	l w	W/
A 100	8.2	0,05 1,00		0,99	N/A	110,0	4.0	0,03	-0.03	0.0227	0.0171	0.0291	2,000	7.5	0.0625	506.4	508.4	501,9	514,9	2,807	1,441	0.00
A101	4.0	0.05 1,00		1,00	15.0	110.0	14.0	0.00	-0.03	0.0727	0,0171	0,0291	2,000	N/A	N/A	506,4	508.4	501,9	514.9	813	342	0.00
A102	3.0	0.05 1.00		1,00	19.0	110,0	21.0	0.03	-0.63	0,0227	0,0171	0.0291	2,000	NIA	N/A	506.4	508,4	501.9	514,9	533	352	0.00
A103	4.0	0.05 1.00		1,00	11.0	110.0	70.4	8,03	-0.03	0.0227	0.0171	0.0291	2,000	1 14/A	. N/A	505,4	506,4	501.9	514.9	550	352	0.00
A 104	4.0	0.05 1.00		1,00	11.0	110.0	:0.4	0.00	-0.03	0.0227	0.0171	0,0291	2,60X		N/A	576,4	500,4	501,9	514,9 514,9	270	189	0.00
A105	2.7	0.05 0.89		1,00	12.0	110.0	£1,7	0.03	-0,03	0,0227	0.0171	0.0291	2,000		N/A N/A	506,4 506,4	508.4 506.4	501,9	514.9	270	169	0.00
A106	2.7	0.05 0.89	1,0	1,00	12.0	110.0	41,7	0.03	-0.03	0,0227	0,0171	0,7291	2,000		N/A			501.9	514.9	135	1 20	0.00
A107	2.0	0.05 0.53	1.0	1,00	11,0	110.0	83.3	0.03	-0,03	0,0227	0.0171	0.0291	5,00		1 N/A	506,4	505.4	501.9	514.9	1,207	768	0.00
A108	[ 4.0	0.05 1.00	1.0	1,00	24.0	110,0	10.6	0.03	-0.03	0.0227	0,6171	0,0291	4,00		NYA	506,4	506,4 511,8	503.0	520,8	533	338	0,0
A109	3,8	0.07 1.00	1.0	0,99	12.0	110.0	21.0	0.03	-0.03	0.0259	0,0180	0.0357	2,00		N/a	500.4	508.4	501.9	514.9	533	343	6,0
A110	3.5	0.05 1.00	1.0	1,00	14,0	110.0	71.0	0.03	-0,03	0.0227	0.0171	0,0291	2,00		N/A		506.4	501.9	514,9	337	42	0.0
A111	1.9	0.05 1.00	1,0	1,00	6.0	110,0	23.3	0,63	-0,03	0.0227	0.0171	0,0291	2,00	N/A	N/A		508.4	501.9		207	132	0.00
A111	2.5	0.05 1.00	1,0	1,00	10,6	130.0	1.0	0.03	~0,03	9,0044	0.0034	9,0056	1 37		1 No.	CONTRACTOR		TERRITOR S. ST			(A)	1996
		PRODUCTOR CONTRACTOR			12 (A) (A)		e de Pariston	1. 19 6 1 14				767	Acceptance of		2.00	LT#15+	The Contract of	140 1 100 100 100 100 100 100 100 100 10	3020 Halle 112			
THE ASSESSED		L DUGGATING GOLDAGOU			al losses						Tarak	LS	One (tonely	T LT	- 1	For	HAT's, 1.5	***				
		der absorptance		(,₩ <b>#</b> ₩	iorking lasse:		٠.				A too	5.6E-0				For	AST's. L	= (days/y	eer in gervi	ce)(VV)(W	V{KE}(K2)	
		apor pressure equali	on .	MV = V:	apor moleculi	x weight					A 101	2.0E-0					For veri	cal tanks,	VV * (PV4)	(D+SKHAQ	)	
		apor pressure equal		N = Nem	riber of turno	vere				200	A 102	1.3E-0				3	For bori	zonial tank	s, W = (P)	/4)(DE^2)(*	(VO)	
	dameter (f			P8# * E	Breather veni	pression s	ethry			54.64 K	A103	1,45.0						* SORT(((1				
		Aponeler (ff)		₽8V # E	Iresther verificant	VICERIM BE	iting :				A 104	1,4E-0				a	Fe	r vertical t	anka, HVO	- 145 - 1礼	+ HPRO	
		eni pressure range		PVA # 1	Vapor pressu	re at averag	pe Sould herry	secutives			44	6.66-4				3		HL = 145				
		A BLEEBERGE LINUGE		PVN * 1	Vapor pressu	ra st min, s	ratace tompo	enture	V 1940	4.0	A105	6.8E-0				8		Por fist	roofs, NRC	) <b>= 0</b>		
		r temp, range, (P)		PVX = 1	Vapor pressu	re of max. I	purface terror	e situa	1.44.5			3.5E-C						For don	ne roofs, H	RO = 0.137	(PCS)	•
4-44-W4 4 u																						
					nuni through	us (hbl/yr)	ī				A107			es Angu	1	<u>.</u>		RS	* 0/2			
HL #1,164	ac height (f	t)		O + Are	Mijeksyft fallyn Eust ffarfis Ane		1				A ton	3.0E-4	3 5.0E-			*		RS	* 0/2	10 = [1/3]	114)	
HL #1,100 HP # T#	uid height (f nk roof heig	i) H (11)		0 * An RS * T:		us (ft)	ī				A109 A109	3.0E-4 9.5E-1	3 5.0E-	03 3.864				RS For com	i = D/2 w roofe, H t = (SR)(Rii	1)		
HL * 1.141 HR * T# HRO * R	uid height (f nk roof heig toof outage	t) Hx (fl) (fl)		0 * Ar RS * T SR * T	ank shell rad	us (ft) I slope	rg :				A109 A109 A110	3.0E-4 9.5E-1 1.3E-1	3 5.0E- 14 2.9E- 13 2.5E-	03 3.8E-0 03 3.8E-0			<b>F</b> r	RS For con	i = D/2 w roofe, H t = (SR)(Rii	1)		
HL # 1.101 HR # T# HRO # F HS # T#	ikk height (f nk roof heig toof oxfage nk ahell heig	t) hx (fl) (fl)		O * And RS * T: SR * T: TB = L: TLA * /	ank ahelt rad ank cone roo igulië bulk ten Average liqui	us (ft) I slope sperature (F ij temperati	## (FI)				A109 A109 A110 A111	3.0E-1 9.5E-1 1.3E-1 1,7E-1	3 5.0E- H 2.9E- 3 2.5E- H 2.5E-	03 3.86-6 03 3.86-6 03 2.76-4			16/6/ m 4/	RS For com His or horizoni LEAPVANA	5 = 0/2 he roofe, H t = (SR)(R5 hi tanks, H f(RVTLA))	() VO = 0.5(1)	1	
HL # 1,kx HR # T# HRO # R HS # Tar HVO = V	uid height (f nk roof heig toof outage nk shell heik rapor space	i Ongađe (U) lye (U) lye (U) lye (U)		O * And RS * T: SR * T: TB = L: TLA * /	ank aheli rad ank cone roo quid bulk len Average Rqui Dally min, liq Dally min, liq	us (ft) I elope iperature (F I temperatu idd surface	re (R) temperiture	(PI)			A109 A109 A110	3.0E-4 9.5E-1 1.3E-1	3 5.0E- H 2.9E- 30 2.5E- H 2.5E-	03 3.86-6 03 3.86-6 03 2.76-4			WV = ((	RS For con His or horizoni MV)(PVA))/ /A = (10"(A	5 = 0/2 14 roofs, H 5 = (SR)(R5 41 tanks, H ((R)(TLA)) - (BI(C + ((	i) VO = 0.5(17) TLA - 492)5	) 9))))(14,7/1	7 <b>6</b> 0)
HL = 1,100 HR = T= HRO = R HS = T= HVO = V KE = V#	uid height (f eik roof heig toof outage nk ahelt heig fapor apace por apace e	t) ht (fl) (fl)   outage (fl)   optage (fl)		O * And RS * T: SR * T: TB = L: TLA * /	ank aheli rad ank cone roo quid bulk len Average Rqui Dally min, liq Dally min, liq	us (ft) I elope iperature (F I temperatu idd surface	re (R) temperiture	(P) (P)			A109 A109 A110 A111	3.054 9.56- 1.36- 1.76- 1.26-	33 5.0E- 14 2.9E- 23 2.5E- 24 2.5E- 34 1.1E-	03 3.86-4 03 3.86-4 03 2.76-4 05 1.36-			WV = ((	RS For con- ## or horizon! Mr/(PVA))/ /A = (10"(A A = 0.44(T/	; # D/2 w roofe, H t = (SR)(R5 w renke, H ((R)(TLA)) - (B/IC + (( VA) + 0.55(1	i) VO = 0.5(17 ILA - 492)5 18) + 0,0071	) 9))))(14,7/1	7 <del>6</del> 0)
HL = 1,100 HR = T= HRO = R HS = Tar HVO = V KE = V# KH = Tu	uid height (f hit, roof heig toof outage hit ahelt heig hapor apace o mover fack	() (A) (A) (A) (A) (A) (A) (A) (A) (A) (		O * A** RS * T: SR * T: TB = L: TLA * : TLX * :	ank aheli rad ank cone roo quid bulk len Average Rqui Dally min, liq Dally min, liq Dally min, liq	us (ft) I slope sperature (F I temperature) uid surface uid surface	re (R) lamparitura lamparitura	(P) (P)			A109 A109 A110 A111	3.054 9.56- 1.36- 1.76- 1.26-	3 5.0E- H 2.9E- 3 2.5E- H 2.5E-	03 3.86-6 03 3.86-6 03 2.76-4			WV = (( p) TI	RS For con- HE or horizoni MV/(PVA)// /A = 0.44(T/ TB = T/	; # 0/2 w roofw, Hi t = (SR)(R5 wi tenks, H ((R)(TLA)) - (BAC + (( WA) + 0.55(T WA + 5(whole)	i) VO = 0.5(17 TLA - 492)5 18) + 0.007 1) - 1	) (9)))))(14,7/1 (akpřin)(1)	
HL # UKK HR # T# HRO # P HS # T# HVO = V KE # V# KK # TU KP # WK	uid height (f ek roof heig toof outage nk ahelf hek fapor apace e mover fack yking foes (	() (A) (A) (A) (A) (A) (A) (A) (A) (A) (	·	O * A** RS * T: RS * T: TB = L: TLA * : TLX * : VLX *	ook ahell radi ank cone roo igule bulk ben Average liqui Dally min, liq Dally man liq Tank man liq	us (ft) I elope sperature (F d temperatu utd surface utd surface utd surface	re (R) temperatura temperatura (N3)	(R) (R)			A109 A109 A110 A111	3.084 9.584 1.384 1.784 1.28	5.0E- 14 2.9E- 2.5E- 2.5E- 2.5E- 34 1.1E- 70TAL	03 3.8E-1 03 2.7E-1 03 1.3E-1 65 1.3E-1			WV = ((	RS For con- He- or horizont Mr/(PVA))/ /A = (10"(A A = 0.44(T/ TB = T/ WhaTV/TLA)	; # D/2 us roofs, H t = (SR)(R5 ul tanks, H ((R)(TLA)) - (Bi(C + (( LA) + 0.55(1 LA + 6(ulpin L+ ((dullum)	i) VO = 6.5(D TLA - 492)S 18) + 0.0071 I) - 1 7 - dellaPf)	) (9)))))(14,7/) (24;21:0)(1) ((PA - PVA))	
AL * Uox HRO * F HS * Tar HVO = V KE * Va KR = Tu KR = Ve KS * Ve	uid heighs (f ek roof heig toof outage nk ahell heik haper space por space e mover fack priding loss ; nted vapor	() (in) (in) (in) (in) (outage	·	G ** Am RS ** Ti SR ** Ti TB = Li TLA ** I TLX ** I VLX **	ank aheli rad ank cone roo quid bulk len Average Rqui Dally min, liq Dally min, liq Dally min, liq	us (ff) I elope operature (F d temperatu old surface old surface old volume olume (fC)	re (R) temperatura temperatura (N3)	(P) (P)			A109 A109 A110 A111	3.084 9.584 1.384 1.784 1.28	5.0E- 14 2.9E- 2.5E- 2.5E- 2.5E- 34 1.1E- 70TAL	03 3.8E-1 03 2.7E-1 03 1.3E-1 65 1.3E-1			WV = () Ti KE = (d	Por com H or horizoni MVX(PVA)) /A = (10"(A A = 0.44(T/ TB = T/ MbTV/TLA)	; # D/2 # roof#, #: # rank#, #: #! rank#, #: ((P)(TLA)) - (B/C + (( MA) + 0.55() MA + 6(### !+ ((d###A)	i) VO = 6.5(D TLA - 492)S 18) + 0.0071 I) - 1 7 - dellaPf)	) (9)))))(14,7/) (24;21:0)(1) ((PA - PVA))	
L * Uck KR * T# KRO * R KS * T# KVO * V KE * V KKH * T# KKH * T# KKH * T#	uid height (f nak roof heig toof oxinge nk ahell heik hapor space por space prover fack oxing loss ; nhed vapor: ph of lank (f	th (fi) (fi) (fi) (h) (h) (h) (h) (h) (h) (h) (h) (h) (h		G * Am RS * Ti SR * Ti SR * Ti TI A * I TI A * I VIX * W * V W * V	ook ahell rad ank cone roo igule bulk ten Average Rigul Dally min. Ili Dally min. Ili Tarli man Ili Tapor space t Vapor danelli	us (ff) slope sperature (F temperature) stemperature sid surface sid surface sid surface sid surface	re (R) temperatura temperatura (RS)	(PC)			A109 A109 A110 A111	13E 13E 13E 12E	50E 9 2.9E 10 2.5E 14 2.5C 14 1.1E TOTAL	03 3.86-4 03 3.86-4 03 2.76-4 05 1.36-			WV = () T1 KE = (d	Por con  He harizoni  MV/(PVA))  A = 0.44(T/  TB = T/  Harv/TLA)  Harv/TLA	: * D/2 * roof*, H ? * (SR)(R5; * tank*, H *((R)(TLA)) - (8(C + f) * (8(C + f) * (4) + 0.56() * (4) + 0.56() * (4) + (4) * (4) * (4) * (4) * (4) * (4) * (5) * (4) * (4) * (4) * (6) * (4) * (4) * (4) * (7) * (4) * (4) * (4) * (6) * (4) * (4) * (7) * (4) * (4) * (8) * (4) * (4) * (8) * (8) * (4) * (8) * (8) * (8) * (8)	i) VO = 6.5(D TLA - 492)5 18) + 0.0071 i) - 1 7 - delt=19) • 0.028(sipt)	) (9))))(14,77) (a4cha)(1) (PA - PVA)) (PA - PVA))	,
L * Uck KR * T# KRO * R KS * T# KVO * V KE * V KKH * T# KKH * T# KKH * T#	uid height (f nak roof heig toof oxinge nk ahell heik hapor space por space prover fack oxing loss ; nhed vapor: ph of lank (f	th (fi) (fi) (fi) (h) (h) (h) (h) (h) (h) (h) (h) (h) (h		G * Am RS * Ti SR * Ti SR * Ti TI A * I TI A * I VIX * W * V W * V	ook ahell rad ank cone roo igule bulk ten Average Rigul Dally min. Ili Dally min. Ili Tarli man Ili Tapor space t Vapor danelli	us (ff) slope sperature (F d temperature) uid surface uid surface uid surface uid surface uid surface uid surface	re (R) temperatura temperatura (RS)	(PC)			A109 A109 A110 A111 DRA	3.0% 9.5% 1.3% 1.4% 1.4%	5.0E 14 2.9E 20 2.5E 24 2.5E 24 1.1E 10TAL	03 3.86- 03 3.86- 03 2.76- 66 126- 8.66-			WV = () T1 KE = (d	Por con  it  iv  rhorizoni  MV/(PVA))  /A = (10"(A  A = 0.44(T/  TE = T/  TE = T/  MaTVTLA)  MaTV = 0.7'  MaTV = PV/(C = 1	; * D/2 w roofw, Hi q = (SR)(R5; wittenks, Hi ((R)(TLA)) - (0)(C + () AA) + 0.56( AA) + 0	i) VO = 0.5(7) TLA - 492)S 18) + 0.0071 I) - 1 / - deltaPff) IC + ((TLX -	) (9))))(14.7/1 (séphe)(1) (PA - PVA)) (H)(1) 492)5(9))))	,
L * i.lq. (R * T * i.lq. (R * i.	uid height (f nik roof heig noof oxinge nik shell heid 'apor space por space a mover fack oxing loss ; nied vapor ith of lank (f anding store	t) ht (n) (n) pht (n) cutage (n) expansion factor product factor ge losses		0 * Am RS * T: SR * T: TE = U: TLA * :: VLX * : VLX * : W * V	onk shell radionik cone roo quid bulk len Average Roth Dally min. Bo Dally mins. Bo Dally mins. Bo Dally mins. Bo Dally mins. Bo Tank max Bo Tank max Bo Tank max Bo Tank max Bo	us (ft) I stope sperature (fi I temperature) I temperature	re (R) temperatura temperatura (RS)	(PC)			A109 A109 A110 A111 DRA	3.054 9.554 1.354 1.25 1.25 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.4	3 5.0E 12 2.9E 22 2.5E 23 2.5E 24 1.1E TOTAL	03 3.86- 03 3.86- 03 2.76- 66 1.26- 8.66-			WV = () T1 KE = (d	Por com or horizont MVX(PVA)) /A = (10°(A A = 0.44(T/A TB = T/A MATV = 0.7: MatV = 0.7: PVX = 1	F D/2 W 1004, H W 1004, H R 1004, H F 1004, H	i) VO = 0.5(I) ILA - 492)5 IB) + 0.0071 I) - 1 I - delta**(I) I) - 0.029(alph I) - (ITLX - 0.234(alph I) - 244(alph I) - 244(alph I) - 244(alph I) - 244(alph I) - 244(alph III - 244(alph	) 19))))(14.7/) (24ptus)(1) (PA - PVA)) 19(1) 49(2)49())))	) K14.7/78
1 * i.lq (R * T * (R * T *) (R * T * (R * T *) (R *) (R * T *) (R	uid height (f nik roof heig noof oxinge nik shell heid 'apor space por space a mover fack oxing loss ; nied vapor ith of lank (f anding store	t) ht (n) (n) pht (n) cutage (n) expansion factor product factor ge losses		0 * Am RS * T: SR * T: TE = U: TLA * :: VLX * : VLX * : W * V	onk shell radionik cone roo quid bulk len Average Roth Dally min. Bo Dally mins. Bo Dally mins. Bo Dally mins. Bo Dally mins. Bo Tank max Bo Tank max Bo Tank max Bo Tank max Bo	us (ft) I stope sperature (fi I temperature) I temperature	re (R) temperatura temperatura (RS)	(PC)		Average	A 109 A 110 A 110 A 110 A 111	3.054 9.554 1.354 1.25 1.25 9.46 Do	3 5.0E 12 2.9E 23 2.5E 24 2.5E 24 1.1E 25 2.5E 25 25 25 25	03 3.86- 03 3.86- 03 2.76- 05 136- 8.06-			WV = () T1 KE = (d	RS For com or horizont MVX(PVA)) /A = (10"(A A = 0.44(T/I TB = T/I MATV = 0.7 MATV = 0.7 PVX = 1 PVM =	F D/2  W 1004, H 1004, H 1004, H 1107,	(C + ((TLM)	(9))))(14,7/) (séphe)(f) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA) (PA	) K14.7/78
L * Liquid HR = T # HRO * F HS * T # HYO * V KE = V KK = V L * Length L * Length	uid height (f nik roof heig noof outage nik aheit heigh apor apace por apace por apace por apace mover fack priding loss ( nited vapor ph of tank (f anding alors priding	(i) (ii) (iii) (iii) (iii) (iii) (iiii) (iii) (iiii) (iii) (iiii) (iii) (i	ie samened	G = Am RS = Ti SR = Ti TI = Li TI A = I TI X = I VLX = V WV = V	onk shell radionik cone roo quid bulk len Average Roth Dally min. Bo Dally mins. Bo Dally mins. Bo Dally mins. Bo Dally mins. Bo Tank max Bo Tank max Bo Tapor spince to Vapor densiti	us (ft) I stope sperature (fi I temperature) I temperature	re (R) temperatura temperatura (RS)	(PC)		Average	A 103 A 110 A 110 DRA	3.05-1 9.55-1 1.35-1 1.25-1 28-2 3/16-Da	3 50E- 1 2.9E- 2 2.5E- 2 2.5E- 2 1.1E- 1.1E- 1.1E- 1.1E- 1.1AX 1.1AX	53 3.85-6 03 3.85-6 03 2.75-6 05 125- 8.66-			WV = () T1 KE = (d	RS For com or horizont MVX(PVA)) /A = (10"(A A = 0.44(T/I TB = T/I MATV = 0.7 MATV = 0.7 PVX = 1 PVM =	F D/2  W 1004, H 1004, H 1004, H 1107,	i) VO = 0.5(I) ILA - 492)5 IB) + 0.0071 I) - 1 I - delta**(I) I) - 0.029(alph I) - (ITLX - 0.234(alph I) - 244(alph I) - 244(alph I) - 244(alph I) - 244(alph I) - 244(alph III - 244(alph	(9))))(14,7/) (séphe)(f) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA) (PA	) K14.7/78
L * Liquid IR * Tar IRO * F IRO * V IRO * V	uid height (f ek roof heig toof outage toof outage ink shell held hepor space of mover fack outage form phof tank (f ending store particular in a mount particular in a mount pa	t)  to (f)  product factor  pr	ie pastymed i	Q = Am RS = TI RS = TI TIA = I TIA = I TIA = I VIX = V W = V	ank shell radi sok cone roo reals bulk ten Average Roof Daily min. So Daily max. So Task max. So fapor space to Vapor dentific sociaries of	us (ft) I slope perature (F I temperature) I temperature Lidd surface	re (R) temperature temperature (R3)	(PC)		Average Average Ambier	A 109 A 109 A 109 DRA	3.05-4 9.55-1 1.35-1 1.25-1 1.25-1 380 Do SNo Do Sn	33 5.0E- 34 2.9E- 33 2.5E- 34 2.5E- 34 1.1E- 35 2.5E- 34 1.1E- 35 2.5E- 36 1.1E- 36 2.5E- 37 2.5E- 38 2.5	63 186-6 63 3.86-6 63 2.76-6 65 126-6 6.66			WV = (() TT FOE = (d) G0	RS For con HE For horizont M/X(PVA)) /A = (10"(A A = 0.44(7) TB = Y/ TB = Y/ MaPV = PV PVX =   PVX =   PVX =   HAPPN = PB	** D/2	i) VO = 0.5(7) TLA - 492)5 18) + 0.0071 i) - 1 7 - delta**(1) 0.029(alphi C + ((TLX - 0.25(delta T (C + (TLX - 0.25(delta T	(9))))(14,7/) (séphe)(f) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA) (PA	) K14.7/78
HE * LIQUED HE TENDE *	uid height (f ek roof heig toof outage toof outage ink shell held hepor space of mover fack outage form phof tank (f ending store particular in a mount particular in a mount pa	(i) (ii) (iii) (iii) (iii) (iii) (iiii) (iii) (iiii) (iii) (iiii) (iii) (i	ie pastymed i	Q = Am RS = Ti SR = Ti TIA = I TLA = I TLX = I VLX = VV = V WV = V WV = V Wo = I Wedge.	ank shell radiank cone roo iguld bulk lan Average Roul Daily min. liq Daily min. liq apor space to vapor densiti actarialics of femos will p	us (ft) slope perature (f themperature) slope sl	re (R) temperature temperature (R3)	(P)		Average Average Average	A 109 A 110 A 111	3.05- 9.55- 1.35- 1.76- 1.26- 370-0-	33 5.0E- 34 2.9E- 33 2.5E- 34 2.5E- 34 1.1E- 35 2.5E- 34 1.1E- 35 2.5E- 36 1.1E- 36 2.5E- 37 2.5E- 38 2.5	33 3.85-6 03 3.85-6 03 2.75- 05 1.25- 8.66-			WV = () FA FA FA FA FA FA FA FA FA FA FA FA FA	POF COMPANY CONTROL OF	; = D02 ; = C02, H2 ; = (SR()(H2, H2, H2, H2, H2, H2, H2, H2, H2, H2,	i) VO = 0.5(7) TLA - 492)5 18) + 0.0071 i) - 1 7 - delta**(1) 0.029(alphi C + ((TLX - 0.25(delta T (C + (TLX - 0.25(delta T	(9))))(14,7/) (séphe)(f) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA)) (PA - PVA) (PA	) K44.7/78
L * Liquid IR * Tar IRO * F IRO * V IRO * V	uid height (f ek roof heig toof outage toof outage ink shell held hepor space of mover fack outage form phof tank (f ending store particular in a mount particular in a mount pa	t) ht (fi) (fi) phi (fi) coutage (fi) wearnation factor product factor saturation factor (fi) get losses (fi) COTHER REPO: inture of all fuels and are fuels to besed on	e sammed product know el temps st	Q = Anv RS = T: SR = T: TR = L: TLA = : VLX = VV = V WV =	ank shell radiank cone roo gould bulk ten Average Rout Daily min. So Daily max. So Tank max. So sapor space to Vapor densiti auctorialists of femps will p	us (ft) slope slope peralture (F f temporati uid surface uid surfa	re (R) temperature temperature (RS)			Average Average Average Ste de	A109 A109 A109 A111 A111 DRA B100 B100 B100 B100 B100 B100 B100 B10	3.05-4 9.55- 1.35- 1.75- 1.25- 3%-00- 9%-00-9%-0	10 5.0E- 10 2.0E- 20 2.5E- 50 1.1E- FOTAL	00 3.85-6 00 3.85-6 00 2.75- 05 1.35- 8.06-			WV = () PN TI FUE = (d di di di V = 0	RS Por com Http: or horizont MV/RVA))/ A = (10"(A	# D/2 # roofs, H  R v (SR)(RS # tanks, H  ((R)(TLA)) - (B/C) + (( AA) + 0.50) AA + 6.60 AA + 6.6	)) VO = 0.5(D  ILA - 492)5 (9) + 0.0071 () - 1 defts**9) + 0.028(skpt) (C.* ((TLX - 1) C.* (	) (9))))(†4.7/) (séphe)(f) ((PA - PVA)) ((PA - PVA)) ((PA - PVA)) ((PA) ((PVA) (PVA)	) (14.7/76
L * Liquid IR * Tar IRO * F IRO * V IRO * V	uid height (f ek roof heig toof outage toof outage ink shell held hepor space of mover fack outage form phof tank (f ending store particular in a mount particular in a mount pa	t) ht (fi) (fi) phi (fi) coutage (fi) wearnation factor product factor saturation factor (fi) get losses (fi) COTHER REPO: inture of all fuels and are fuels to besed on	e sammed product know el temps st	Q = Anv RS = T: SR = T: TR = L: TLA = : VLX = VV = V WV =	ank shell radiank cone roo gould bulk ten Average Rout Daily min. So Daily max. So Tank max. So sapor space to Vapor densiti auctorialists of femps will p	us (ft) slope slope peralture (F f temporati uid surface uid surfa	re (R) temperature temperature (RS)			Average Average Steeles	A 109 A 109 A 110 A 110 A 111 A 110 A 111 A 110 A 111	3.05-4 9.55-1 1.75-1 1.76-1 1.26-2 3.00-1 3.	10 5.0E- 10 2.0E- 20 2.5E- 50 1.1E- FOTAL	00 3.85-00 00 3.85-00 00 2.75-00 05 1.35- 8.05-		v	WV = () PN TI FUE = (d di di di V = 0	RS Por com Http: or horizont MV/RVA))/ A = (10"(A	# D/2 # roofs, H  R v (SR)(RS # tanks, H  ((R)(TLA)) - (B/C) + (( AA) + 0.50) AA + 6.60 AA + 6.6	)) VO = 0.5(D  ILA - 492)5 (9) + 0.0071 () - 1 defts**9) + 0.028(skpt) (C.* ((TLX - 1) C.* (	) (9))))(†4.7/) (séphe)(f) ((PA - PVA)) ((PA - PVA)) ((PA - PVA)) ((PA) ((PVA) (PVA)	) K44.7/76
L * Liquid IR * Tar IRO * F IRO * V IRO * V	uid height (f ek roof heig toof outage toof outage ink shell held hepor space of mover fack outage form phof tank (f ending store particular in a mount particular in a mount pa	t) ht (fi) (fi) phi (fi) coutage (fi) wearnation factor product factor saturation factor (fi) get losses (fi) COTHER REPO: inture of all fuels and are fuels to besed on	e sammed product know el temps st	Q = Anv RS = T: SR = T: TR = L: TLA = : VLX = VV = V WV =	ank shell radiank cone roo gould bulk ten Average Rout Daily min. So Daily max. So Tank max. So sapor space to Vapor densiti auctorialists of femps will p	us (ft) slope slope peralture (F f temporati uid surface uid surfa	re (R) temperature temperature (RS)				A 103 A 103 A 110 A 111 W DRA DRA DRA DRA DRA DRA DRA DRA DRA DRA	3.05-4 9.55-1 1.35-1.76-1.26-1.26-1.26-1.26-1.26-1.26-1.26-1.2	10 5.0E- 10 2.0E- 20 2.5E- 50 1.1E- FOTAL	53 3.RE- 53 3.RE- 53 2.PE- 60 1.3E- 8.0E- 9 9 3 3 3 4 4 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1			WV # (() P\ TI FOE = (d) d) d (S = 1) FOE = (T) FOE = (T	RS For com For	# D02 # 1006 # 1	)) VO = 0.5(D TLA - 492)5 18) + 0.0071 1) - 1 1 - deltaPH) + 0.020(alph (C + ((TLX - 0.25(delta T C + ((TLA - 0.25(delta T	  (aspin)(14.77)  (aspin)(1)  (PA - PVA))  (PA - PVA)  (PA - PVA)  (PA - PVA)  (ASZ)SES))))  (ASZ)SES))))	) (14.7/76
L * Liquid IR * Tar IRO * F IRO * V IRO * V	uid height (f ek roof heig toof outage toof outage ink shell held hepor space of mover fack outage form phof tank (f ending store particular in a mount particular in a mount pa	t) ht (fi) (fi) phi (fi) coutage (fi) wearnation factor product factor saturation factor (fi) get losses (fi) COTHER REPO: inture of all fuels and are fuels to besed on	e sammed product know el temps st	Q = Anv RS = T: SR = T: TR = L: TLA = : VLX = VV = V WV =	ank shell radiank cone roo iguld bulk lan Average Roul Daily min. liq Daily min. liq apor space to vapor densiti actarialics of femos will p	us (ft) slope slope peralture (F f temporati uid surface uid surfa	re (R) temperature temperature (RS)			4 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	A 109 A 109 A 110 A 110 A 111 A 110 A 111 A 110 A 111	3.05-4 9.55-1 1.75-1.76-1 1.26-1 38-0 Site Demographie (F) white (	10 5.0E- 10 2.0E- 20 2.5E- 50 1.1E- FOTAL	53 3.RE- 53 3.RE- 53 2.PE- 60 1.3E- 8.0E- 9 9 3 3 3 4 4 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1		v	WV # (() P\ TI FOE = (d) d) d (S = 1) FOE = (T) FOE = (T	RS For com For	# D02 # 1006 # 1	)) VO = 0.5(D  ILA - 492)5 (9) + 0.0071 () - 1 defts**9) + 0.028(skpt) (C.* ((TLX - 1) C.* (	  (aspin)(14.77)  (aspin)(1)  (PA - PVA))  (PA - PVA)  (PA - PVA)  (PA - PVA)  (ASZ)SES))))  (ASZ)SES))))	) K44.7/78

Red vapor presure, gendes

#De 18/19/20 Sci (DONY) 82 - 2010 Figed vapor presure, crufts of

Padd vapor presure, crufts of

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	T		Tank s	he#				Floaling								NOR	ihwest te			WY		1
	B 1	nstruc-			Color	Туре	Construc-	4	Seal typ				.		_			ello terv		HEOMANA		1
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			Light r		belge,	pontoen,		Machanie		Shoe mo			1				UPDATES	October 1	<b>6</b> , 2001			1
		elded or	dense		błack, gray	or double	Welderf or	, Savid mo		igu tubra				<u>-</u>						FF I		
Tank		veted	Or Bisupt		or white	deck	holted		nounted	weather		Contr		A	- 8 .		CF	0	FC	·	KC	0.00
902		Velded	Light		White	Internal	Welded		novinted	N//		Sign		6.805	1283.50	273,1	0.0015	42.5	1.0	288	1.0	
904		Vetded	Light		White	Internal	Welded		nounted	N/i	· · · · · · · · · · · · · · · · · · ·	Sepre		8,805	1263,50	273,1	0.0015	42.5	1.0	288	1,0	0.00
907		Verted	Light		White	Internal	Welded		nounted	PAG NA		HS Die		2,642	358,22	99.9	0,0015	42.5	1.0	288	1.0	0.00
909		Veided	Light		White	internat	Wekled		nounled	NI NI		Md-G		8,805	1283.50	273.	0.0015	40.0	1.0	283	1,0	0.00
910		Velded	Light		White	Inlemal	Wekted	<del></del>	mounted	N/		Md-G		6.805	1263.50	273.1	0,0015	40,0	1.0	283	1.0	0.00
911		Melded	Light		White	Internal	Melded		mounted	Ni Ni		Unle		8,805	1283,50	273,1	0.0018	56,5	1.0	317	1.0	0.00
913		Welded Welded	L light		White	Internal	Welded	<del></del>	mounted		/A.	Supr		6,805	1263,50	273.1	0.0015	40.0	1.0	283	1,0	0.00
913 914		Welded	Light Light		White	Internal	Welded		mounted		1 <u>4</u>		aded	6,805	1263.50	273.1	0,0015	40.0	1,0	283	1.0	0,00
915		Welded		rusi	White	Internal	Welded		mounted				-Bittell	8.805	1283.50	273,1	0,0015	48.0	1.0	299	1.0	0,00
915		Welded		rusi I rest	White	internati miemai	Welded		mounted		/A		aded	6.806	1283,50	273,1	0,0015	40.0	1.0	283	1,0	0.00
918		Welded		t rust	White	Internal	Welded	···	mounted		)/A	<del></del>	arted	8,805	1263.50	273.1	0,0015	52.5	1.0	308	1,0	0,00
919		Welded		t rusi	White	Internal	Bolted	— · · · · · · · · · · · · · · · · · · ·	mounted				aded	8,805	1263.50	273,1	0.0015	56,5	1.0	317	1,0	0,00
920		Welded		i rusi	White	Internal			mounted		xxmled		esef #2	2.842	358,22	99,9	0.0015	60.0	1.0	360	1.0	0,34
10000	177 10	TTO LOCK	ST TO STATE OF THE			Suite Light	Bolled	* VB000	mounted		ounled		aded	8,805	1283,50	273.1	0,0015	60,0	1,0	360	1.0	0,34
1	4		4						行為中國					7.3				14 - A - A - A - A - A - A - A - A - A -	क्षा क्षा क्षा क्षा कर	4.1.1.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	APPENDENCE OF THE	NAME OF THE OWNER, OWNE
Tani	-	KRa	KRb	MV	-	NC NC	P	PVA	CT THE REAL PROPERTY.	Action 10 and 10		****	-				<u> </u>			s (lons per )		·
902		6.7	N/A	88.0	N/A	<u> </u>	0.0942	3,9455	10	0.20	TS	TSI		Mr			Yark	LD	LF	LR	LWO	LT
904		6.7	N/A	66,0	N/A	+			244,242		506.4	0.0	0,0	6.2	- 45		902	0.0E+00			2.86-02	
907		8.7	N/A	130.0		<del></del>	0.0942	0.0040	243,894	0.20	508.4	0.0	0.0	8.2	-15 7.000	0.14	904	0.0E+00			2,65-02	
909		5.7	N/A	56.0	N/A	+	0,0001		385,790		506.4		4	7.0	- 1		907	0.06+00			4.6E-02	
910		5.7	N/A	66.0	N/A	+	0.0942		346,565 347,224	0.20	506.4 506.4	0,0	0.0	6.2			909	0.0E+00			3.9E-02	
911			N/A	66.0	N/A	<del></del>	0.0942				506.4	0.0		6.2	-13/23/25		910	0.05+00			3.9E-02	
912		6,7 6.7	N/A	66.0	N/A	<u> </u>	0.0942		1,574,367 270,694	0.20	506.4	0.0	0.0	6.2	-		011 012	0.0E+00			1.2€-01 3.0€-02	
			N/A	4	N/A	<del></del>			744,107	0.20	506.4	0.0	0.0	6.2	- 3		913					
913		8.7	<u> </u>	66.0	N/A		0.0942				506.4	0.0	0.0	8.2	- 65	100	914	0.0E+00				
914		6.7	N/A	66,0		<u> </u>	0.0942		404,128	0,20	508.4	0.0	•		- 120		915	0.0E+00				
915		6.7	N/A	66.0	N/A	<u> </u>	0,0947		744,078			0.0	0.0	6,2		500	915	0.0E+00				
916		6,7	NIA	66.0	N/A	<u> </u>	0.0942		1,339,310		506.4	0.0	0.0		- 72		R18	0.05+00				
918		6,7	N/A	66.0	N/A		0.0942		1,574,837	0.20	508.4 508.4	0.0	0.0	7.0	- 196		919	1.3€-0:				
919		2.2	N/A	130.0			0,0001	10,0040	964,963 1,034,386		506.4	0.0	0.0	6.2			920	0.76				2 2,
920		2.2	N/A	66.0	N/A	1	0,0942	3.9455	1,0,16,286	1 0,20	-20/10.*	((,t)	- 10 MAY 18 MAY	90000000000000000000000000000000000000			A REPORT				,	
30.70	7 21 2			~ 2.0			(A)													≹l πα	)TAL	1 23
	2.4	100	/ <b></b>		Site Da								S 20 HU		200	2.50		12.00	41.00			1
40					mperature (		46		XATANY2		10.72	4.0						444	100	1000	SPISSION !	76.20
2		4			ure (F) # TA						4.7		A # Cons	tant in van	or gressare :	ectation	The second second	LT = Tola	loss			
	gui 18				## (F) # TAR		33			10.2	1200	- Jan			OF SYMBSONS			LWD + W	/IIhdrawal k	285		
2					re range (F)		25 10		A WALLSON		4.4				OF DIRECTOR			MV = AVE	. vapor mo	lecular welg	hit, Kulito-moli	ie
100	100				d (mph) = Y		4.4		<b>**</b>	New Year					factor, bbl/1					apeed exp		
	* 1		Site eleve							A STATE OF THE STATE OF	20.5			demater.				NC = No	mber of fixe	d roof colun	at supports	
		112.74			ric pressure	(psta) * PA	12		1						nn diameter,	ŧ		P * Vapo	r prossure i	function		
			Solar Insc				1,5			the market					ig loss facto		•	PVA + Va	BOOK DEBSSU	re al sionag	e temp, pak	•
2.1			ideal gas				10.7						R L	oduci factor		,			rail throught			
244	10.4				re, gasoline			10 (18)	FATTA TO	<b>文表。</b>	3.00			ck seem to				SD = D#0	k seam len	ight factor, f	M2	
	32.1		Reld vep	or pressur	re, crude of			$\Delta = 0$							eed fim sea	loss factor	r	TS = AV	KADO SOUF	al atock term	perature, R	
100		中的海		- 1- V	<b>地流发</b> 性		STATE OF THE STATE OF	工 次 清			200				dent ilm seo					esk terrep, de		ajcs.
		WO+LF						1276			1.00			ck seem to			-			med at teck		
	R = (	KR# + (()	(K\$PK^.u.)))	(₽ΧΩΧ <sub>IV</sub> ν	/KC)						740.20			ok filling had				WL = Av	өгждө огдан	nic Nauki de	nuty, ibigai	
		For Inter	nal floating	roofs, v	- 0					170			diam me.									
1		P = (PVA	/PAY(1 + (1	~{PVA/P	A))*0.5}*2				PATER	4	100			1277.00	Control No.	<b>3</b>		Carlotte State	462		*11.2.1 P	State Control
1		PV	<b>≒ # {10^(</b> A -	(B/(C+(	(15 - 492)6/	9)))) <u>)</u> (†4.7/7	(DC)		<b>107</b> (107)		1.00	1.0	ASSUM	PTIONS A	ID OTHER!	NFO:						
			TS - TA	+ TSI								3.55	th Cons	ه ۱۱۸۳ محک	examed to s	verzoe 10.	O. Data sug	gests the in	ne avelade	to be 9.6.		
1	WD.	<b>= (((0.94</b> )	KOKCEKA	LIYDX1	+ (((NCXFC	)YD))			<b>多世级</b>		A 18 18 18	中国	7) Vers	e melacida	weight (MV	is for fast	lerros at 50	F. Lower N	empe produ	ce lower M	/a.	
		FFYPYM							1	28.77			2 31 4	ene skronk	hade cross	ere based o	n sila eleval	fion."				
l i	D + 1	KDXSO	D-ZXPXM	/XKC)					4	*****			<b>All</b>			ها کمین بشد.	managed by	have character	cleristics of	gesoline.		
		100		10000		***	<b>***</b>	1000年1000年1000日	THE PERSON NAMED IN	(10)	Carlo Barrier	With the contract	11,000		774-24					1.7	Terr (218)	5. X. S. S. S.

Note: Throughputs are based on allowable throughputs shown in Tier if Permit Application, dated April 2, 2001, plus throughput increase expected as a result of adding DRA to system, which is expected to increase gesoline by 186,000 gallons and dieset by 32,000 gallons.

FF - Total deck fitting loss factor, ib-mole/vr FF = 10ral beck fitting loss factor, 0-moley/r
KF7? = loss factors for a particular type of deck fitting
KF8 = zero wind speed loss factor for a fitting type
KFD = wind speed depandent loss factor for a fitting type

Kv = fitting wind speed correction factor

(NFsh)(KFsh) + (NFcw)(KFcw) + ... + (NFw)(KFw)
For external Rosters, KF77 = KFs + (KFb)((Kv)(v))^m) Kv = 0,7 For Internal Roaters, KF27 = KF9

	1				Acces	s haids			
Tank	FF		Bolled or unbolled	Gaskeled or ungaskeled	KFah	KFå	KFb		NFah
902	288,0573		Unbolled	Ungaskeled	38	36	N/A	N/A	1
904	288.0573		Unboited	Ungasketed	36	36	N/A	N/A	<del>                                     </del>
907	288.0573		Unbolled	Ungaskeled	38	35	N/A	N/A	<del>                                     </del>
60.6	283,3667		Unbolled	Ungasketed	36	36	N/A	N/A	<del>                                     </del>
910	283,3667	<b>表面和</b>	Unbolled	Ungaskeled	36	36	N/A	N/A	<del>                                     </del>
911	317,3863		Unbolled	Ungasketed	36	36	N/A	NrA	<del></del>
912	283,3867		Unbolled	Ungaskefed	36	36.	N/A	N/A	<del> </del>
913	283,3667	1	Unbolled	Ungaskeled	36	36	N/A	N/A	<del> </del>
914	298,956		Unhoited	Ungasketed	36	36	N/A	N/A	<del>                                     </del>
915	283,3867	a with	Unbolled	Ungaskeled	38	38	N/A	N/A	1
916	308,4656	100	Unbolled	Ungaskeled	36	36	N/A	N/A	<del></del>
918	317,3663	1072	Unbolled	Ungaskeled	36	36	N/A	N/A	
919	360.06	120	Unbolled	Ungaskeled	38	36	N/A	N/A	1
920	380,08	Little Control	Unbolled	Ungaskeled	36	36	N/A	N/A	<del></del>

Round pipe or bilitalp column	Gaskeled sliding cover, or langaskeled sliding cover, or flexible fabric sleeve seal	KFcw	KFa	NFo
Выйчир сочитт	Ungasketed silding cover	47	47	13
Beit-up cohimn	Ungasketed sliding cover	47	47	1
Bull-up cokerns	Ungaskeled sliding cover	47	47	1
Bulk-up column	Umgaskeled sliding cover	47	47	1
Brigg-Filb Copiumis	Ungaşkeled sliding cover	47	47	+
Вий-ир сочини	Ungaskeled sliding cover	47	47	+
Euilli-185 CONSTIN	Ungaskeled stiding cover	47	47	1 1
Bulli-tip cokima	Unuskeled silding cover	47	47	1
Brigg-nith cupitimu	Ungaskeled sliding cover	47	47	1 1
Bull-193 column	Ungaskeled sliding cover	67	47	1 7
Вий-ир сочит	Ungaskeled sliding cover	47	47	1
Ви <del>й нэр сохутп</del>	Ungaskeled sading cover	47	47	1 1
Ви#-ир соция	Ungasketed sliding cover	47	47	1 1
Bulli-up column	Ungasketed siking cover	47	47	1 1

			Gridepoles at	nd sample v	velte :	Marian Articl		
Tank	Unaloffed or slotted	Skding cover Gaskeled, or Ungaskeled	w/ Pole sleave, pole wiper, float, float/wiper, or float/wiper/sleave	KFgp	KFa	KFb	<b>.</b>	NFoo
902	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
904	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
907	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
909	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
910	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
911	N/A	NA	N/A	N/A	N/A	N/A	N/A	1
912	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
913	NIA	N/A	N/A	N/A	N/A	N/A	N/A	1
914	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
915	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1
916	N/A	Gaskeled	N/A	N/A	N/A	N/A	- N/A	1
918	N/A	Gaskeled	Float/wiper/steeve	N/A	<b>N</b> FA	N/A	N/A	1
919	N/A	N/A	N/A	N/A	NIA	N/A	N/A	1
920	N/A	N/A	N/A	N/A	NIA	N/A	NIA	1

		GBUCG-	cel well	······································		
Bolfed or unbolfed	Gaskeled or ungaskeled	KFqf	K₽a	KFb	m	NFor
Inbolled	Ungasketed	1 74	14	N/A	N/A	14-04
Unbolled	Ungaskeled /	14	16	N/A	N/A	<del></del>
bettodni	Ungaskeled ,	14	14	N/A	N/A	<del>                                     </del>
Unbolled	Ungaskeled	14	. 14	N/A	N/A	1
Unbolled	Ungaskeled	14	14	N/A	N/A	1
Unholled	Ungaskeled	14	14	N/A	N/A	1
Unbolled	Ungasketed	14	14	N/A	N/A	1
Unholled	Ungaskeled	14	\$ <b>4</b>	N/A	N/A	1
Unbolled	Ungaskeled .	14	14	N/A	N/A	1
Unbolled	Ungaskeled	14	14	N/A	N/A	1
Unbotted	Ungasketed +	14	14	N/A	N/A	1
Unhohed	Ungaskeled	14	14	N/A	N/A	1 1
Unbolled	Ungasketed	14	14	N/A	N/A	1
Unboffed	Ungaskeled	14	14	N/A	N/A	1

1		Gauge	halchham	ole port		
Tank	Gaskeled, ungaskeled, or sill fabric seal	KFgh	KFa	KFb	· m	NiFgf
902	Sit fabric seal	12	12	N/A	N/A	1 "
904	S#I fabric seal	12	12	N/A	N/A	1
907	SR fabric seal	12	12	N/A	N/A	1
909	SR fabric seaf.	12	12	N/A	N/A	1
910	5# fabric seal	12	12	NIA	NA	1
911	SM fabric seat	12	12	N/A	N/A	1
912	5Rt fabric seel	12	12	N/A	N/A	1
913	S# fabric seal	12	12	N/A	NA	1
914	SR fabric seal	12	12	N/A	NIA	
915	Silf fabric seel	12	12	N/A	N/A	1
916	SR fabric seal	12	12	N/A	NUA.	1:
918	SM fabric seal	12	12	N/A	N/A	1
910	S# fabric seel	12	12	N/A	N/A	
920	SM fabric seal	12	12	N/A	N/A	

Deck drains; open, Deck drains; closed, or stuti drains	KFdd	KF2	KFb		NFdd
N/A	N/A	NA	N/A	N/A	14
N/A	N/A	N/A	N/A	NA	14
N/A	N/A	N/A	N/A	N/A	14
N/A	N/A	N/A	N/A	N/A	13
. N/A	N/A	M/A	N/A	N/A	13
N/A	N/A	N/A	N/A	N/A	26
N/A	M/W	NA	N/A	N/A	13
N/A	N/A	N/A	N/A	N/A	13
, N/A	N/A	N/A	N/A	N/A	18
N/A	N/A	N/A	N/A	N/A	13
N/A	N/A	NA	N/A	N/A	22
N/A	N/A	N/A	N/A	N/A :	26
Skib drains	1.2	1.2	N/A	N/A	29
Stuit: dreine	1.2	1.2	NA	N/A .	29

<u>1</u>			***************************************	***************************************	······································	:		t	leck legs			7					4.		
r						· · · · · · · · · · · · · · · · · · ·					E	demat ponto	on deck						
1								Po	ntoon area						. (	Jewler stes			
- 1						ſ	Gasketed						Gaske	1	-		j l		
- 1	Adkistable			Ot existing:	double deci		ungaskete		- 1	ļ	1	1	ungaske	ated,			1	l	ï
Tank	or fixed	KFdI	KFa	KFb	75%	, NFd	or sock	· K##	KF2	K#b	#	NFdI	<b>0</b> f 80		KFdi	¥₹a	KFb .	<u></u>	NFdt
902	Adjustable	7,9	7.9	N/A	N/A	12	NIA	M/A	NIA	N/A	N/A	N/A	N/a		N/A	" N#A	E N/A	N/A	N/A
904	Adjustable	7.9	7.0	NA	N/A	: 12	NIA	N/A	N/A	N/A	NIA	N/A	N/A		N/A	N/A	N/A	N/A	N/A
907	Adjustable	7.9	7.0	N/A	N/A	12	N/A	NIA	N/A	N/A	NIA	5N/A	N//		N∕A	N/A	N/A	N/A	NA
909	Adjustable	7,9	7,9	N/A	Nik	12	M/A	N/A	N/A	NIA	N/A	NIA	N#	,	N/A	N/A	.: N/A	N/A	N/A
910	Adjustable	7,9	7.9	N/A	NIA	12	N/A	NIA	NIA	N/A	NIA	N/A	N/	Q.	N/A	N/A	: N/A	N/A	N/A
911	Adhistable	7.9	7.9	N/A	N/A	16	N/A	N/A	N/A	N/A	N/A	NIA	N/	Α	N/A	N/A	· N/A	N/A	NIA
812	Adjustable	7,9	7,9	N/A	N/A	12	N/A	N/A	N/A	N/A	NIA	N/A	N/	Ą	N/A	N/A	N/A	N/A	N/A
913	Adjustable	7.9	7.0	N/A	N/A	12	N/A	N/A	N/A	N/A	NIA	NIA	N	A	N/A	NIA	N/A	N/A	NIA
Q14	Adjustable	7.9	7.9	N/A	N#A	14	N/A	N/A	N/A	N/A	N/A	N/A	N.		N/A	N/A	: N/A	NIA	N/A
915	Adjustable	7,9	7,9	N/A	N/A	12	N/A	N/A	N/A	NJ/A	N/A	ATTA	N		N/A	N/A		N/A	N/A
916	Adjustable	7.9	7,9	N/A	N/A	15	NIA	N/A	N/A	N/A	N/A	N/A	N N		N/A	N/A	N/A N/A	N/A	N//
918	Adjustable	7.9	7.8	N/A	NIA	. 16	N/A	N/A	N/A	N/A	NIA	N/A	N		N/A	N/A			N/
919	Adjustable	7.9	7,9	N/A	N/A	17	NIA	N/A	N/A	N/A	N/A	N/A	<u></u> N		N/A	N/A	N/A N/A	N/A N/A	N//
920	Adkistable	7,9	7.9	N/A	N/A	8 17	N/A	\$3/\$	Al/A	5178	1 kilk				<del></del>	<del></del>			N//
			753 PRO 1/2			TEXTS IN		The Contract		No. of Concession,	77 F. FE	m N/A N/A N/A		TOTAL SE	SAN SPECIA	NIA	NIA	N/A	
		٧,	acutem brea	kers.				The second section of the second	walter State of Table	Pire vent	tioned deliberation	i sentina seka (ili anto)				701113	Ladder w		4
	Gasketed or	T	T	T T	T	1		Gasketed or	T	T	1	<del></del>	<del></del> -		9	keled or	Cauca M	<u> </u>	7
Tank	umpasketed	KF√b	KFa	KFS	l "	NFvb	200	unpasketed	KFIV	KFa	l k₽h		Men	200	3 300	aereu ur eskeled	KFIW	KFa	NF
902	Gasketed	6.2	6.2	N/A	N/A	1 1		N/A	N/A	N/A	N/A	N/A	10777	2	t loo	askeled	78	78	<del></del>
904	Gasketed	8.2	6.2	N/A	N/A	13.1		N/A	N/A	N/A	N/A	N/A	<del>                                     </del>		ki thon	asketed	78	78	1
907	Gasketed	6.2	6.2	N/A	N/A	13 1	150 (200)	N/A	N/A	N/A	N/A	3 N/A	1		Linc	eskeled	78	76	1 1
909	Gaskeled	6.2	6.2	N/A	N/A	1 1		N/A	N/A	N/A	N/A	IN/A	1 1		Line	askeled	78	78	1
910	Gasketed	6.2	6.2	N/A	N/A	+		N/A	N/A	N/A	N/A	N/A	1 -			askeled	78	78	1
B11	Gasketed	6.2	6.2	N/A	N/A	+		N/A	N/A	N/A	N/A	N/A	1			askeled	78	78	1 1
912	Gasketed	6.2	6.2	N/A	N/A	1 2 1		N/A	N/A	N/A	N/A	N/A	<del> </del>	327	1100	askeled	76	76-	1
913	Gaskeled	6.2	8.2	N/A	N/A			N/A	N/A	N/A	N/A	N/A	1 1	医多类	· · · · · · · · · · · · · · · · · · ·	asketed	76	78	1 7
914	Gasketed	6.2	8.2	N/A	N/A	+		N/A	N/A	N/A	N/A	; N/A	<del>                                     </del>		V. ************************************	paskered	76	76	1
				N/A	N/A			N/A	N/A	N/A	N/A	M/A	<del>1</del>		# <del> </del>	raskeled	78	78	
915	Gaskeled	8.2	6.2				- 1	N/A	NEA	N/A	N/A	N/A	+ + +			zasketed :	. 76	76	1
918	Gaskeled	6.2	6.2	N/A	N/A	1 1		5115	N/A	N/A	N/A	N/A	<del>                                     </del>	- W.W.G		asketed	76	76	
918	Gasketed	6.2	6.2	N/A	N/A	<u> </u>		N/A N/A	N/A N/A	N/A	N/A	N/A	+		El III	pasketed	75	76	1-
919	Gasketed	6.2	8.2	N/A	N/A	1 1		N/A		N/A N/A	N/A	N/A	<del></del>	1800		anskeled	78	1 78	1
920	Gaskeind	6.2	6.2	N/A	N/A	1 1		NA	N/A	] NA	l NA	N/A		1900 100 100 100	G1 UN7	Sesionary			

and a grain on lawye. The otherwise and

Programme Company

# POCATELLO TERMINAL POTENTIAL FUGITIVE VOC EMISSIONS UPDATED October 16, 2001

Source	Service	Number	Emission	Émissions
		Of Units	Factor*	(Tons/Yr)
Valv <b>es</b>	Liquid .	1,089	9.48E-05	0.45
Valves	Vapor	30	2.87E-05	3.8E-03
Fittings	Liquid	902	1.76E-05	7.0E-02
Fitting <b>s</b>	Vapor	100	9.26E-05	4.1E-02
Pump Seals		41	1.19E-03	0.21
Others	Liquid	87	2.87E-04	0.11
•	,	тотл	AL.	0.89

\*Table 2-3 Marketing Terminal Average Emission Factors, Protocol for Equipment Leak Emission Estimates, EPA-453/R-95-017, November 1995 Emissions = (# of units)(emission factor)(hours/day)(365)/2000

Emissions = (# of units)(emission factor)(hours/day)(365)/2000

Number of valves is actual times 1.1

Number of fittings is actual times 1.1

Number of pump seals is actual

Number of others is actual times 1.1

Actual counts increased to accomodate possible overlooked sources.

Truck loading fugitive emissions accounted for in the valves and fittings listed as in vapor service.

### **APPENDIX C**

## **Toxic Air Pollutant Emission Estimates**

#### MORTHWEST TERMINALLING COMPANY POCATELLO TERMINAL POTENTIAL EMISSIONS SUMMARY AND HAP DATA UPDATED October 16, 2001

PASIUMP TURNS AND UTHER RYFO;

1) Maintenance assumed to add an additional 2% to the total facility emissions.

2) HAP concentrations as specified in HAP tegend.

3) Yapor destruction and (VOU) natural gas burn VOC's are accounted for in the truck lossing section, while HAP's are not. Current usage averages 43 SCF per Nou.

50	ONT PER VEAR! WE	Potential								WOLF HADD (		. 1						Total
		VOCs [		107-02-8		71-43-2		1319-77-3		100-41-4			91-20-3	108-95-2	100-42-5	106-85-3		HAPs
Hive so			or alone				at No.		16/36/84		AM . S			***		100		<b>建</b>
Velves.		0,45				5.9E-03		1,46.03	4,5E.04	5,26-03	5.7E-03		1.2E-03	2.4E-03	1.9E-94	2.4€-02	2,9E-02	7.RE-02
Valves	- vapor	3.66-00]				8.9E-04		2.36-07	2.7E-05	6,8E-05	1.55-03	,	3.3E-07	8.7E-07	1,8E-06	1.06-03		3,8E-0:
Fittings		7,0E-02				9.16-04		2.1E-04	7,0E-05	8,0E-04	8.9E-04		1.96-04	3,76-04	2,96-05	3,8E-03		
Fillings	+ VRÇOF	4, 1E-02.				9.56-03		2.5E-06	2.9E-05	7.3E-84	1.6E-02		3,5E-06	7.2E-06	1.7E-05	1,16,-02	3.7E-03	4,1E-0
Pump !		0.21			11	2.8E-03		0.4E-0#	2.1E-04	2.4E-03	2.7E-03	i	5.7E-0#	1,15-03	8,85,-05	1.9E-02	1.4E-02	3.5E-0
Others	, Neppiel	0,11			1	1,45,03		3.38-64	1,1E-0#	1,36-03	1.4E-03	<u></u>	2.98-04	3,85-04	4.5E-05	5.96-03	7.0E-03	1.8E-0
Ϋ́t	TAL.	0.89	0.06+90	0.06+00	0.0€+00	2.1E-02	9,0€,+00	2.5E-03	1,7E-04	1,0E-02		0.05-00	2.35.63			5.7E-02		
ixed roof	tarks -	230 27 274	E Rooke Va	Service Services	10000000	34 43 Value	A. 16. 16. 16. 16. 16. 16. 16. 16. 16. 16	9 S 10 E 3 P	38 Mile	a contractor		32 C 17 C	J. (2) (1)			TO HER		
901	LS Diese #1	4.4E-02				1,35-03	3.3E-06	9.65-06	1.96-04	4,55-04		8.0 7.03	4.8E-05	1.7E-05				
0	LS Olesel #2	9.56,-02		1	1	3.76-03	7.2E-06	Z.1E-05	4.1E-04	9.KE-04		1.7E-02	1.0E-04		2.6E-05	1.3E-02		
903	LS Dienei #1	4,4E-02		<del>1</del>	1	1,56-03	3.3E-05	9.5E-06	1,96-04	4.5E-04		8.1E-03						
0	MS Diese #2	7.5E-02	1	1	1	2.6E-03	5.7E-08	1,8E-05	3.2E-04	7.7E-04		1.4E-02	4.8E-05	1.7E-0		1.3E-02		
905	HS Diesel #2	1,16-01		<del>                                     </del>	<del>-}</del>	3,66-03	8.6E-06	2.4E-05	4.8E-04				<b>₹.26-0</b> 5			2.2E-02		
906	LS Diesel #1	4,46-02		<del>†</del>	<del> </del>	1.5E-03	3.3E-06		1,9E-04	1,26-0; 4,56-0		2.1E-02	1.2E-04			3.4€-07		
0	LS Diesel #2	9.5E-02		<del>                                     </del>	<del></del>	·····				********		8.1E-03	4,86-05			1.3E-07		
908	HS Diesel #2	1.16-01		<del></del>	<del>-}</del>	3,26-03	7,2E-06	2.15-05	4,18-04	9,#E-04		1,75-02	1,0E-04			2.8E-02		
917	LS Diesel #2	0.25		<del> </del>	-{	3.6E-03	8.5E-09		4,85-04	1,16-0:		2.05-02	1,2E-04			3.3E-0		
930	Transmia			-	<b></b>	0.5E-03	1.9E-05		1,1E-03	2,66-0		4,65-02	2.7E-04					
		2.3E-0;		<del></del>	ļ	5.5E-03	ļ	1.48-08	1,7E-05	1.72-0			2.0E-06					
-5300	Transmiz	6,1E-0		<u> </u>	<b></b>	9.7E-04	<u> </u>	2.5E-07	2,96-06	7,4E-0:			3,85-07					
-3000	Transmix	2.4E-00		1		5.7E-04	<u> </u>	1.5E-07	1,7E+06	#,3E-0			2,1E-07	4.3E-0	1.0E-06	8.5E-0	4 2.2E-0	4 2.46-
-5000	Transmis	3.3E-0:		1		7.9E-04		2.0E-07	2,46-06	6.0E-©	5 1.3E-03		2.9€-07	7 5.9E-0	7 1.4E-06	8.9E-0		
A100	OGA 493Q	8,1E-00	3	1				1	2.6E-0#							1	1,4E-0	3 1.7E-
A101	TFA 4904	4.5E-0.	3	1						1,7E-0	5						1,6E-0	
A102	Starreon	3,8E-0	3)	1			1	]		j · · · · · · · · · · · · · · · · · · ·	1	J	4,4E-0	B.	· ]	1	1	4,46-
A103	Guardian	3,9€-0	3	T	<u> </u>		1	1			1	1	1.5E-0	5		1	6.78-0	M 6.8E-
Atna	OGA 591	3.DE-0.			<u> </u>	<u> </u>	<del> </del>	1	1,3E-04	· · · · · · · · · · · · · · · · · · ·	<del>- }</del>	·		" <del>                                     </del>	<del></del>	<b>—</b>	6,7E-0	34 8,0E-
A105	HITEC 4983	2.9E-0		<del></del>	<del></del>	<del></del>	·	<del> </del>	9.8E-05	2.1E-0	51		2.2E-0	7		1	2.7E-0	
A106	Valve Master	2.9E-0		<del>-  </del>	<del></del>	···	·	1		<u> </u>	~	<del>1</del>	<u> </u>	<del>`</del>	<del></del>	1	1	0.0E+
A107	Peradyna 870	1,7E-0		<del>-1</del>		<del></del>	<del>1</del>			<del> </del>	· · · · · · · · · · · · · · · · · · ·	<del></del>	6.3E-0	e e		·		8.3E
			~-	<del>·</del> {	· <del>  · · · · · · · · · · · · · · · · · ·</del>	<del> </del>	- <del></del>	·	2.7€-04	<del>}</del>	<del>- </del>	<del> </del>				1	1.4E-0	1.7E
A108	OGA 401W	8.0E-0		_	<del></del>	<del></del>	. <del>ļ</del>	- <del> </del>	2.150	<del> </del>	<del></del>	· <del> </del>	Į		<del> </del>	+		0.064
A109	1€7ec 4103	3,85-0				. <del>j</del>	<del></del>	-		ļ	<del>- }</del>	<del></del>	<del> </del>		<del>- }</del>	<del> </del>		0.0E
A110	Phase V	3.8E-0				<u> </u>		<b></b>		5.7E-0		-	<del> </del>	<del>-1</del>		·•	2.1E-4	
Att	Red Dye	2.7E-0			<u></u>	<u> </u>		<u>-</u>	<del></del>	8154	<u> </u>	- <del>{</del>	·	<del></del>				0.00
DRA	DRA	1,3E-0		<u></u>		<del> </del>	<del></del>	1,96.04	4,5E-63	1,08.4	1.0E-01	1,8E-01	1.7E-0	4 3.4E-4	4 5.2E-0	4 0,2	27 1.4E-	
,	TOTAL	0.9							T . E		Septime :			100				
Floating	roof tanks	AS YEAR		4									1,1E-0					77. 231. 10. 10. 11. 11. 1
902	Supreme	1,6	31			1,0€-0		1.2E-04	2,6E-0									
904	Supreme	1,8				1.0E-0		1.26.04	2.86.0				1,16-0					Territoria (1977)
907	HS Diese #2	4.9E-0				1,15-0			3.9€-0				1,00.4 1,8E.4					
909	Mid-Grade	1,7	75]			1,0E-0		1,85-04	3.3E-0									
910	Mid-Grade	1.1		ŀ		1.0E-0		1,86-04	3.3E-0				1.8E-0					
911	Unleaded	2.7		<u> </u>		1,4E-0		5.8E-04	0,4E-0				8.0E-4					
912	Sepreme	1.7				9,9€-0	3	1,45,04	2.8E-0				1.76-					
	Unleaded	1			<u> </u>	1,18.0	2	3.8E-04	5.8E-0				3,4#.4					
913		1.1		1	<del>-  </del>	1,1E-0		1,76-04					1.5E-4					
914	Supreme	1 - 1				1,1E-0		3.66-04					3.4E-4					
915	Unleaded	7.		-1	1	1.36-0		5.76-04	7.7E-0				4.6E-4					
918	Unleaded					1.45.4		5,6E-04	8.4E-0	5 3.7E			5,0E-4					
918	Unleaded	2.				1,56-(				5 9.1E-	05 4,2E-0	# 7.4E-0						
919	LS Diesel #2	8.55				1.45-(		3.5E-04	<del></del>				3.1€.					
920	Uniceded	2,:									02 0.2	4 1.3E-0	3,7E4	03 6,65			.22 1.2E	
	TOTAL	23	.7 0.0E+	0.0E+	0.0E+0	0.1	∓ . },⊅K-4					V COMPANY			<b>建</b> 多分和高			
Truck in	ading VOU Stack	2.22	August 2-4	of the Later					1.06.0				3.1E			04 1.0E-	-01 3.2E	
Gas		<b>†5.</b>	47			8.5E-4		2.2E-C	_				3.46					
Tran		3.96-	02			9.3E-0		2.4E-0										-01 1,01
Dies		1.3E+				4.3E.4		2.9E-0	3.66-0	3 1.45	02 1.35-4	<u> </u>	4.26-			1.4E		
		See non		28 3.15	06 \$,7E-0				1			C 2.4E-0			04 9.SE-			.23
144	raf Gas Usage TOTAL	11				4 8,	4 1,0E-				82 8.3							0#
						0.3	10	5.2E-0	6.0E-4	<b>4</b> ]	ez #.1	3 <u>1</u>	7.IE-	na! 1'96.	<u></u>	<u> </u>		
			5.22															
	Maintenance				<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>	_1					, o (BO	9.4	e #.5E-		02 2.9€-		.20 0	.62

		Weight fraction of component ( in the liquid, to Mo (211.)														
,	Acet- sideliyde	Acroleln	Forin- aldeflyde	Benzene	Siphenyl	Cresci	Comena	Emyl- benzene	n-Hexane	MTBE	Naph- tratene	Phenol	Styreise	Tokene	Xylonea	
Stream Description	75-07-0	107-02-8	50-09-0	71-43-2	92-52-4	1319-77-3	98-82-8	100-41-4	110-54-3	1634-04-4	91-26-3	108-95-2	100-42-5 j	108-88-3	1030-20-7	Tol
rventional Gesoline (ell grades)		i		1,806-62	0	4,52E-03	5,80E-04	1,80E-02	1.90E-02	0 ]	3.99E-03	7.85E-03	6.22E-04	0.22E-02	6,68E-02 -	2.4
ygensted Conventional Gasoline				1,80E-02	0	4,57E-03	\$,50%-04	1,非0在-02	1.00E-02	1,50E-01	3,996-83	7,85E-03	6.22E-04	#.22€-02	8,686-02	3,9
esel No. 2, No. 1, Heating Fuel				1,77E-04	1.21E-03	1,05E-03	5.75E-04	6,30E-04	3.146-04	3,35E-(M	3.27€-03	1,12E-03	5.396-05	5.74E-03	9.51E-03	2,4
rude Öf				3.03#-63	0	1,37E-03	1.02E-03	1,80E-03	9,37E-03	5,33E-03	7,45E-04	1,256-04	8,94%-04	5.27E-03	7.84E-03	3.6
Friel, Commercial Jet Fuel, JP-8				7.69E-03	4,446-03	2.78E-03	1,136-03	2.95E-03	1,72E-02	O	6.38E-03	3,14E-03	9.85E-04	2.04E-02	1,385-02	8,1
Sulluni X				1.306-02	0	3,90E-03	1,006-03	1,15E-02	1.27E-02	0	2.70E-03	5,30E-03	4,13E-04	5,406-02	8.40E-02	1.8
steral Gae (ZI,V)	3.53E-02	1,31E-02	4,09E-02	1,85E-02		<u></u>					1,79E-01			5.90E-03	2.20E-03	2.9
AP weight fraction data comes from CRTC.	•			5,905	7,9524	6,811	6.963	6.975	6,676	6,85249	7,3729	7,133	7,14	8.954	7,84014	1
Natural gas data comes from Radian Corp. 8		<u> </u>	1211,033	2599,62	1435.5	1480,793	\$424,255	1171,17	1103,737	1968.36	1515,79	1574,51	1344,8	2090.32	]	
Natural Gas emission factors are libs, per million of of gas burned. C		Same and the same	720.79	256	165.46	207,78	213.21	224,45	222.72	222.51	174,95	224,09	219,48	273.16	٦	
			M	79,11	154.21	108,14	170.19	108,17	65.16	88	128.17	94,11	104,15	92,14	108,17	1
Conventional Gasoline (all grades)	T ML	100	T 0	0.790	2,52E-04	8,05E-04	1 3.01E-02	6,64E-02	1,328	T 11						
	MV	68	1-5	1.826-02	0.006+00		1.40E-05	1,12E-03	3,706-02	2.262 0,00E+00	1,33E-03 4,13E-06	1,34E-03	4,386-02	0.213	6,18E-02	4
	WL	8.2	1 +	2.31E-02	0.00E+00		1.656-01	1,896-02	2.79E-02	0.00E+00	3.11E-03	**************************************	2.51E-05	1.90€-02	5:06E-03	4
	PVA	3.9455	T i	4.82E-03	0.00E+00			2.84E-04	9.38E-03	0.006+00		8,34E-03	5.97E-04	8.92E-02	8:18E-02	
	TA	#.O	ZV	5.47E-03						0.00E+00	1,05E-05	2,83E-06	8.836-06	4.81E-03	1.285-03	[
Oxygenated Conventional Gasoline	1,41	100		+ 2276723	1 0.00	1,400,000	0.416-00	1 4,50C,*U4	\$ 3.05E-03	0.000	2.U3E-48	4.04E-06	1.05E-05	8.72E-03	2.06E-03	_
	W	56	1-5-	··-	- <b>ļ</b>	<del></del>	<del>-</del>	- <del> </del>	<del>-}</del>		<del> </del>	<u> </u>	ļ		<u> </u>	4
This material is not located at this facility,	Wi.	6.2			···	- <del></del>	4	1	-4		<u> </u>	<u> </u>	<b>ļ</b>		<del>                                     </del>	-Ì
	PVA		1 %	- <b> </b>			<del></del>	<del></del>	<del> </del>	<del> </del>		1	ļ	<u> </u>		
	TLA	<del> </del>	1 - <u>X</u> V	·••	•••	···	~ <del> </del>	<del> </del>	<del> </del>	<del></del>	·•	<del> </del>	<del> </del>	<del></del>	. <b></b>	
N	I.H.	130	<del>                                     </del>	0.930	-	+	+		1	1	<u> </u>	<u> </u>		<del> </del>	<u> </u>	-
Diesel No. 2, No. 1, Healing Fuel	MV.	130			2.73E-04			7,07E-02		2.355	1,44E-03	1,48E-03	4,88E-02		6.54E-02	
			<b>P</b> 4	2.45E-04				1 71 - 11 -		1,17E-03	4,76E-08	2.29E-06	3.145-08		7,70E-04	
	WL		<u> </u>	2,95E-04							3.315-03	1.55E-03	6.736-05	****		-4
	P\/A	0.0043	y#i	5.68E-02						0.271	1,106-03	5.29E-04	7.27E-04		0,175	[
	TA	8.9	ZĻV	3.41E-02	7,62E-05	2,18E-04	4,29E-00	1.03E-02	- 0,101	0,183	1.09E-03	3,83E-64	5.83E-04	0.299	0,148	
Crude Oli	ML.	675	Р.								<u></u>	<u> </u>	1	<u> </u>	<u> </u>	
	W	50	<b>7</b> 4					1			4		ļ		1	
This material is not located at this facility.	Wt.	7.7	対								4		<u> </u>	_	<u> </u>	
	PVA		γ.				<u>. I</u>	_ <u>j</u>				.1	<u> </u>		<u> </u>	
	TLA		ZU,Υ				1				<u> </u>					
Jet Fuel, Commercial Jet Fuel, JP-8	\$4	130	P						1		ļ		<b>_</b>		<u> </u>	
	WV	130	PI	1						1		1	<b>_</b>	<u> </u>		
This material is not located at this facility.	WL	8.7	×				1			<u> </u>	<u> </u>	<u>.</u>				
	PVA	<u> </u>							<u>.   : </u>			<u> </u>	4			[
	PVA		¥.			1									<u> </u>	
	TLA		2.V	" I				1					1	<u>.</u>		_
	L#	100	7 7	0.880	2.89E-0	4 9.61E-0	3.38E-07	7,39E-0	1,437	2.442	1,52E-03				6.825-0	
Tementalia.	W	86	Pi	1,43E-0			3 2.81E-0	BOIE A	2.58E-0							
	WŁ	<del>  ~</del> -	1	1.88E-0				1,08E-0	2 1,865-0		2,11E-00					
	PVA	0.0193	1 7	0.741	0.00E+0				2 1.384		1.66E-04				0.213	
	TIA	9.5	ZiV	0.876	0.00€+		4 2.85E-0	3 6.00E-0	1,430	0.000-0	3.22E-04	8.50E-04	1.56E-0	3 0.991	0.342	1

A = constant to vapor pressure equation, dimensionless

B \* constant in vapor pressure equation, degrees C

C \* constant in vapor pressure equation, degrees C

LD = dack seem losses, lb/yr

LF = mod fitting losses. Relyr

LR = rim see losses, b/yr

T = total losses, the

LTI = amission rate of component i, bye (fixed)

LTI = amission rate of component i, bye (fixed)

LWD # withdrawal losses, lb/yr

AR = molecular weight of component i, Ruth-mole IRL = molecular weight of Roard stock, forth-mole IRV = molecular weight of vapor stock, Ruth-mole

P w vapor pressure of component i at liquid surface temperature, puts

P) \* pertal pressure of component i, pels PVA = total vapor pressure of liquid mixture, psis TLA - average tiquid surface temperature, degrees C at a liquid mote fraction of component i, its mote/fo-mote

y = vapor mole fraction of component i, ib-mole/th-mole 2), = weight fraction of component i in the liquid, ib/fis

ZLV = weight fraction of component I in the vapor, lb/E

For Auditive sources - Sould, LTI = (2LL)(LT)
For Southing root tends, LTI = (2LV)(LR + LF + LD) + (2LL)(LWD)
For all other sources, LTI = (2LV)(LT)
ZLV = ((V)(DAT))AAV = (10°(A - (BATLA + C)))(0.0183306)(2LL)(ARL)FVAAAV)
yl = PAFVA

Pt = (P)(xt) P = (10/(A - (B/(TLA + C)))(0.0193300)

M = SZLIMATIAN

. Additions			14 P's	CAS#	ZŅL	A		Č I	妈
GA 493Q	Mt.	130	Comene	98-82-8	2.00E-02	6,953	1460,793	207,78	120,19
•	MV	110	Xylene	1330-20-7	5.00E-02	7,94014	2090.32	273,16	106,17
	WL	7,71		1					
	PVA	0.023							
A 4904	TLA	9,1				. 1			********
-A 4904	<u> </u>	130	Ethyloenzene	100-41-4	1,00E-03	6,975	1424.255	213.21	108,17
	.w/	110	Xylene	1330-20-7	1.00E-02	7,94014	2090,32	273.16	108,17
	WŁ	7,71		_1					·
	PVA	0.023							
farrece	TA	9,1							
HETTER	<b>1.4</b>	130	Naphthalene	91-20-3	1,50E-02	7.3729	1968.38	222.81	128,17
	WV	110	· · ·						120,31
	W.	7.64					! · · · · · · · · · · · · · · · · · · ·		<del> </del> -
	PVA	0.023						<del></del>	<del> </del>
Reprison	TLA.	9.1				····			<del></del>
Schle (Stille)	M,	130	Naphihalene	91-20-3	\$,00E-02	7,3729	1988,36	222.61	1
	W.	110	Xylene	1330-20-7	5.00E-02		2090,32	273.18	128.17
	W.	7,71					4020,04	213.70	106,17
	PVA	0.023					<del> </del>	i	<del> </del>
)GA 581	T.A.	9,1				······································	<u> </u>	<del></del>	<del>}</del>
JOH SET	<u>ut</u>	130	Cumene	96-62-8	2,00E-02	8.963	1490,793	207,78	120,19
	140/	118	Xylene	1330-20-7	5.00€-02		2090,32	273.16	106.17
	. vn	7,71					1	TALLEY.	100.37
	PVA	0.023	<del></del>				<u> </u>		<del></del>
97ac 4980	T.A	9.1					<u> </u>		Ī
स । सम्ब चक्का¥	<u>M.</u>	130	Current	94-52-6	2.00E-02	6,963	1450,793	207,70	120,10
	W/	110	Ellytheraux;	100-61-4	2.00E-03	5,975	1474.255	213,21	105,17
	WI.	7,71	Naphtialene	91-20-3	1,006-03		1968,36	222,81	128,17
	1 WA	6,023	Xylene	1330-20-7	2.70E-02	7,94014	2090,32	273,18	106,17
/dva Master		9.1							
LEAST MINERAL	M,	130	<u> </u>						1
	MV	110	<u> </u>						
	W.	7.71	<u> </u>						
	PVA	0.023	<u> </u>				<u> </u>		
	T.A	9,4	<u> </u>					[	E
Paradyne 570	M.	130	Naphthelere'	91-20-3	5.006-02	7.3729	1988,38	222.61	128,17
	MV	110					Í		
	LAV	110	. T				Ī		T
	WL	7.71					]		1
	PVA	8.023							<u> </u>
	TLA.	9,1							L
DGA 401W	M.	130	Cumene	96-82-8			1460,793	207,78	120.11
	MV	110	Xylene	1330-20-7	\$.00E-02	7,94014	2090,32	273.18	108.17
	WL.	7,37	1						
	PVA	0.023	- 3		[				
	7.4	9,1	<u> </u>		<u></u>	<u></u>	<u> </u>		1
HT4c 4103	M.	130	<u> </u>			ļ	ļ	<b></b>	1
	M/	110				<u></u>		<b></b>	<u> </u>
	W.	7.43	<u> </u>			<u> </u>		<b></b>	4
	PVA	0,028	<u> </u>		<b>ļ</b>	<del> </del>		<u> </u>	<b></b>
	TA	11.0					<u> </u>	<u> </u>	<u> </u>
7:46¢ V	144.	130				<u> </u>	<u> </u>	<u> </u>	
	NV.	110					<u> </u>	1	1
	WL	7,34						1	
	PVA	0,023	1			<u> </u>		<u> </u>	
	TLA	9,1				I			
Red 8 - 50	148,	130	Ethylograpane	100-41-4	1,35E-01	8,975	1424,255	213.21	106,1
···	MV	110	Xylenes	1330-20-7			2000,32	273.16	100.1
	WL	8,26	T					I	
	FVA	0.023	T			T			

1	. 1	Ethy4	Nach-	1
1	Cumena	benzene	malene	Xytene
· p	3.27E-02	***************************************		5 63F-02
\$74	7,07E-04			4,05E-03
μž	2,166-02	<del>"</del>	······································	0.126-02
Y	3,12E-02	···	· · · · · · · · · · · · · · · · · · ·	0.179
Z),V	3.41E-02			0,173
<b>#</b>	[	7.17E-02		6.635-02
PA		8.78E-05		8,12E-04
¥4	1	1.22E-03		1,27E-02
74	ļ	3.87E-03		3.58E-02
Zi,V		3.74E-03		3.485-02
Þ		01770700		3.460-04
Pl	<del> </del>		1.48E-03	<u> </u>
	<del>}</del>		2.22E-05	
yd	<u> </u>		5,52E-02	]]
Z,V	<u> </u>		9.82E-04	
	ļ	<u> </u>	1,145-03	
<del>p</del>	<del> </del>		1,465-03	5.63E-02
	<del></del>	<u> </u>	7,426-05	4.06E-03
<u>xi</u>	<del> </del>	<u> </u>	3,07E:02	8,12E-02
<u>y</u>	<del> </del>	<u> </u>	3.27E-03	0,179
Z,V	1	<u> </u>	3,82E-03	0,173
E9	3.27E-02	<u> </u>	1	8.43E-02
	7,07E-04 2,16E-02	<del> </del>	<u> </u>	4,08E-03
	3,12E-02	<del> </del>	<u> </u>	6.12E-02 0.179
20,7	3,41E-02	<del> </del> -		0.173
	3.27E-02	7,17E-62	4 445 75	
F4	7.07E-04	1,76E-04	1,48E-08	6.63E-02 2.19E-03
Y	2.16E-02	2.45E-03	1.016-03	3.31E-02
¥	3,12E-02	7.75E-03	8.55E-05	9.67E-02
Z,V	3,41E-02	7,486-03	7.63E-05	9.34E-02
p		1	1	
<b>55</b>	<u> </u>	<del></del>	<del>                                     </del>	·
мł	1	Ţ <del></del>	<del>                                     </del>	<u> </u>
y		1	<del>                                     </del>	
z,v			1	İ
P	]	1	1,486-03	·
174		<u> </u>	7.42E-05	1
P4	1	1	2.43E-07	1
x)	1	1	5.07E-07	†~~~~
γ.		1	3.27E-03	<del> </del>
ZI,V		i	3.82E-03	
ţp.	3,27E-02	ì	1	6,63E-02
124	7.07E-04		I	4.06E-03
16	2,185-02			6.126-02
ᇲ	3.12E-02	1	L	6.179
	3.41E-02			0.173
<u> </u>	<u> </u>	1	4	
	_ <b></b>	<u> </u>	4	
<u>*†</u>		<u> </u>	<b>-</b>	.ļ
_ <del></del>	<del>-[</del>	<del> </del>	<del> </del>	<del></del>
Z.V		<del></del>	<del>-{</del>	
-		· <u></u>	<del></del>	
Pi	<u> </u>	<b>-</b>	<u> </u>	
ᆏ				<del> </del>
<u> </u>		<u> </u>		
ZI,V				
P		7,17E-02		6.63E-02
件		1,18E-02		4,38E-02
Ħ.	1	0.165		0.861
άν		0,523		1,935
ZV		0.505	1	1,867

Where a concentration runge is given in the MSDS, high end of runge is fieled.